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REBOCA, SL is a company with $100 \%$ Spanish capital, which was founded in 1981 having as its main activity the recovery and recycling of plastic materials.

After some time, the company began to diversify its product range, entering the drip irrigation fittings and piping market. Little by little, the offer of fittings was extended, until in 1985, REBOCA, SL begins to manufacture piping for the supply of pressurised water.

This represents a major growth for the company since the service to clients is not only provided in terms of piping, but also in relation to all fittings necessary for the installation assembly, both of irrigation and pressurised water.

While the company grows in this sense, it abandons the recovery and recycling of materials, in order to be able to focus its efforts on piping manufacture.

In 1992, the random polypropylene (PP-R), piping and fittings for the pressurised hot and cold water pipeline, for heating, cooling, hot water system, sanitary water and water for human consumption REPOLEN product range was added to our catalogue.

In 1994 an entire line of piping and fittings made in high-density polyethylene (PE-100) for pressurised cold water pipelines, sanitary water and water for human consumption, recycled water, gas, hydrocarbons; joined by polyfusion with socket system was added, obtaining a complete range of products easy to install and with the same connection technique. This made it possible to complete the offer for installations.

Since then and until now, REBOCA, S.L. has been working on PE-32 and PE-40 pipe manufacture for irrigation and pressure, PE-100 for pressurised cold water and PP-R for pressurised cold and hot water, as well as the necessary fittings.

In January 2001, the Company Registration Certificate according to UNE-EN ISO 9001 was granted by AENOR. At the end of March of the same year, the AENOR N mark was granted for PP-R pipe manufacture in our facilities in L'Ollería (Valencia).

- In December of the same year, the AENOR N mark for PE-100 pipe manufacture was obtained.
. In June 2002 the AENOR N mark for PE-40 and PE-32 pipes for microirrigation was obtained.
The PP-R fittings are certified in 2007
- In 2009 the REPOLEN PP-R system is certified.
- In 2010, DNV certification for PE-100 and PP-R and AENOR N certification for PE-100 and PP-R batteries and manifolds were obtained - In 2011, the AENOR N mark for PE-100 gas pipes is obtained.

In 2013, the AENOR N certification for PE-RT (temperature resistant polyethylene) pipes for heating water and radiant floor was obtained.
In 2015 , the Faser multilayer (PP-R / PP-R with fibre glass / PP-R) pipe for pressurised hot water, cooling and hot water system certification was obtained.

Currently and by exclusive decision of REBOCA, S.L. and under commercial criteria, the following certifications are maintained:

\author{

- Pp-R pipes
PP-R Fittings <br> - REPOLEN system in PP-R <br> - PE-100 pipes for water <br> - PE-100 pipes for gas <br> - PE-40 Pipes <br> - Faser Multilayer Tubes
}

One of the main concerns of REBOCA, S.L. has been and continues to be to offer our clients products with the highest quality, for this purpose we have been adapting our facilities and our products catalogue to their needs.


### 2.1 APPLICATION STANDARDS

$\square$ UNE IN 1555 : Plastics piping systems for the supply of gaseous fuels. Polyethylene (PE)
UNE IN 12201: Plastics piping systems for water supply Polyethylene (PE)

- UNE IN ISO 15874: Plastics piping systems for hot and cold water installations Polypropylene (PP)

UNE 53394 IN: Plastics. Code for the installation and handling of polyethylene (PE) pipes for water piping under pressure. Recommended Techniques

- UNE 53943: Plastic networks to centralise water meters. Polyethylene (PE), polypropylene (PP) and polybutylene (PB) networks with butt welded joints RP 001.01: Specific AENOR N marking regulations for polyethylene (PE) pipes for water supply and sanitation under pressure.
- RP 001.52: Specific AENOR N marking regulations for plastic piping systems for hot and cold water installations.

RP 001.72: Specific regulations for the AENOR certificate of conformity for polypropylene (PP-R) and fibreglass (FV) piping systems for hot and cold water installations inside the structure of buildings.

RP 01.73: Specific AENOR N marking regulations for polyethylene (PE) fittings for the supply of gaseous fuels.

## 22 REFERENCE DOCUMENTS

- CTE: Technical Building Code
- RITE: Regulation of Thermal Installations in Buildings

ISO 9001: Quality management systems. Requirements
ISO 14001: Environmental management systems. Requirements with guidance for use
$\square$ UNE 53943: Plastic networks to centralise water meters. Polyethylene (PE), polypropylene (PP) and polybutylene (PB) networks with butt welded joints

- UNE 53959 IN: Plastics. Thermoplastics pipes and fittings for the transport of liquids under pressure. Calculation of head losses

UNE-EN 476: General requirements for components used in discharge pipes, drains and sewers for gravity systems UNE-EN 752: Drain and sewer systems outside buildings
UNE-EN 805: Water supply - Requirements for systems and components outside buildings
UNE-EN 806: Specifications for installations inside buildings conveying water for human consumption
UNE-EN 1295: Structural design of buried pipelines under various conditions of loading.
UNE-EN 1610: Installation and testing of sewage connections and networks.
UNE-EN 12666: Plastics piping systems for non-pressure underground drainage and sewerage Polyethylene (PE)

- UNE-EN 13244: Plastics piping systems for buried and above-ground pressure systems for water for general purposes, drainage and sewerage - Polyethylene (PE)

UNE-EN 13476: Plastics piping systems for non-pressure underground drainage and sewerage Structured-wall piping systems of unplasticised
$\square$ poly(vinyl chloride) (PVC-U), polypropylene (PP) and polyethylene (PE)
UNE-EN 13689: Guidance on the classification and design of plastics piping systems used for renovation
UNE-EN 14409: Plastics piping systems for renovation of underground water supply networks
UNE-EN 50086: Conduit systems for cable management
UNE-EN ISO 15494: Plastics piping systems for industrial applications. Polybutene (PB), polyethylene (PE), and polypropylene (PP). Specifications $\square$ for components and the system. Metric Series

UNE-ENV 12108: Plastics piping systems Guidance for the installation inside buildings of pressure piping systems for hot and cold water intended
$\square$ for human consumption
Polyethylene piping. Technical Manual. ASETUB

■ Equipment for the control of the fluidity index

- Eq

Equipment for controlling the contents of fibre glass, ashes, carbon black, etc.
Dimensional inspection equipment (inner and outer caliper, circrometer, micrometer, magnifying glass)

- Equipment for water tightness control
- Equipment for longitudinal shrinkage control

Equipment for resistance to cracking control
Equipment for tensile test control

- Equipment for impact resistance control

Equipment for internal pressure resistance control

$\square$ Product Certificates
$\square$ Product compliance certificates


PIPELINES


The REPOLEN* system used in hydro-sanitary installations, following the guidelines indicated in the Technical Manual, is covered by an insurance policy contracted by REBOCA, S.L. TRANSFORMADOS PLASTICOS; with the company GROUPAMA; Policy no. $63,132,771$ for a value of 1,202,040 euros.
$\square$ The conditions governing this warranty are:
Send the warranty certificate within 10 days of completion of the installation.
The pipes and fittings must be installed following the instructions, warnings, and recommendations contained in the REPOLEN ${ }^{\circ}$ Technical Manual. Insurance coverage will be for 10 years from the date of production marked on the pipe and fittings. Within this time frame, damages up to $1,202,040$ euros, caused both to objects or people, by the breakage of a REPOLEN* pipe or fitting with manufacturing defects, will be compensated.

The warranty is not valid in the following cases:
The connection between the pipe and the fitting, with heat source with temperature and pressure limits, even if accidental, is not compatible with the features of the material used by the REPOLEN ${ }^{*}$ system.
Failure to follow the instructions for use, warnings, and recommendations in the REPOLEN ${ }^{\circ}$ Technical Manual
Use of obviously defective materials (cracked pipes and fittings, etc.)
Use of components not manufactured by REPOLEN* / REBOCA, S.L. for the execution of the installation

- Incorrect or defective welding due to the use of unsuitable fittings.


## Instructions for Claiming Warranty Intervention:

In the event of damage attributable to the pipe or fitting, and only for the reasons described above, you must inform REBOCA, S.L. by registered letter of the type of damage and send the damaged piece of pipe or the fitting, as well as a copy of the Warranty Certificate, which must

## include

- Place and date of installation.
- Name and address of the installer
- Marking of the pipe or fitting, if possible on the product or on the container.

After receiving the above in our Company, within a reasonable time frame, our company will make the necessary arrangements and transfer the
documentation received to the Insurance Company.

Any payment made by REBOCA, S.L. to carry out the procedures with the Insurance Company will be borne by the claimant, if the reasons for the breakage are not those foreseen within the warranty.



MATERIAL


PROPERTIES

### 4.1 TYPES OF POLYPROPYLENES

Polypropylene is a polymer formed by monomeric high molecular weight chains of propylene, which gives excellent mechanical properties, making it suitable for both hot and cold water installations.
Depending on the type of monomers and their molecular arrangement, three types of polypropylene can be identified:

- PP-H (polypropylene Homopolymer). It only has propylene monomers. It is not suitable for human consumption water, nor for pressurised cold water use. It is therefore used for transporting hot water, sewerage drain, industrial fluids, etc.
- PP-B (polypropylene block). It has propylene and ethylene monomers arranged by blocks in polymer chains. It is very resistant to impact, even at low temperatures but does not have much pressure resistance. It is not suitable for human consumption water. It is used little and basically for drainage.
- PP-R (polypropylene random). The propylene and ethylene monomers are randomly arranged in the chains, providing very good mechanical properties, especially under pressure with or without temperature. Suitable for human consumption water.


### 4.2 PHYSICAL MECHANICAL PROPERTIES

REPOLEN* piping and fittings are manufactured with type 3 Polypropylene Random Copolymer, a very high molecular weight propylene and ethylene REPOLEN ${ }^{\circ}$ piping and fittings are manufactured with type 3 Polypropylene Random Copolymer, avery high molecular weight propylene and ethylene
copolymer with a random arrangement of monomers, with excellent mechanical resistance up to $100^{\circ} \mathrm{C}$ and an exceptional chemical resistance that makes it the best system for transporting food liquids and other hot fluids under pressure.

It also has a high resistance, which ensures easy handing for installation and transport even at temperatures below $0^{\circ} \mathrm{C}$.

| PROPERTY | value | UNITS | TEST PROCEDURE |
| :---: | :---: | :---: | :---: |
| Fluidity Index ( $230^{\circ} \mathrm{C} ; 2.16 \mathrm{~kg}$ ) | 0.3 | gr/10 min | ISO 1133 |
| Fluidity Index ( $230^{\circ} \mathrm{C} ; 5 \mathrm{~kg}$ ) | 1.2 | $\mathrm{gr} / 10 \mathrm{~min}$ | ISO 1133 |
| Density at $23^{\circ} \mathrm{C}$ | 905 | Kg/m3 | ISO 1183 |
| Elastic Flexural Modulus | 815 | MPa | ISO 178 |
| Charpy impact resistance with notch, $23^{\circ} \mathrm{C}$ | >9 | kJ/m2 | ISO 179 |
| Tensile strength at the Yield point | 34 | MPa | ISO 527-2 |
| Tensile strength at the breaking point | 27 | MPa | ISO 527-2 |
| Elongation at the breaking point | > 520 | \% | ISO 527-2 |
| VICAT, 9.8 N | 70 | ${ }^{\circ} \mathrm{C}$ | ISO 306 |
| HDT 0.45 MPa | 45 | ${ }^{\circ} \mathrm{C}$ | ISO 75 |
| Long-term hydrostatic resistance after 50 years and $20^{\circ} \mathrm{C}(97.5 \% \mathrm{LCL})$, MRS | > 8.0 | MPa | ISO TR 9080 |
| Fire Classification. Multilayer Faser pipe. Halogen free | B2 | --- | DIN 4102 |



CHEMICAL RESISTANCE 4.3


# PRODUCT 


5.1 Single-layer PPR pipes according to UNE-EN ISO 15874
5.2 Three-layer FASER pipes according to UNE-EN ISO 15874
5.3 Fittings

### 5.1 SINGLE-LAYER PPR PIPES ACCORDING TO

(1)

| S5 SDR11 PN10 application classes/design pressure: 4/6; 2/4; 1/6 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Nominal diameer (mm) | Internal diameer (mm) | Thickness (mm) | Weight (kg/m) | Capacity (1/m) |
| 20 | 16.2 | 1.9-2.2 | 0.11 | 0.21 |
| 25 | 20.4 | 2.3-2.7 | 0.17 | 0.33 |
| 32 | 26.2 | 2.9-3.3 | 0.27 | 0.54 |
| 40 | 32.6 | 3.7-4.2 | 0.42 | 0.83 |
| 50 | 40.8 | $4.6-5.2$ | 0.67 | 1.31 |
| 63 | 51.4 | 5.8-6.5 | 1.04 | 2.07 |
| 75 | 61.4 | 6.8 - 7.6 | 1.45 | 2.97 |
| 90 | 73.6 | 8.2-9.2 | 2.09 | 4.25 |
| 110 | 90 | 10-11.1 | 3.11 | 6.36 |
| 125 | 102.7 | 11.4-12.7 | 3.28 | 8.2 |
| 160 | 130.8 | 14.6-16.2 | 6.6 | 13.44 |

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| S3.2 SDR7.4 PN16 application classes/design pressure: 5/6; 4/10; 2/6; 1/8 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Nominal diameter (mm) | Internal diameter (mm) | Thickness (mm) | Weight (kg/m) | Capacity (1/m) |
| 16 | 11.6 | 2.2-2.6 | 0.09 | 0.1 |
| 20 | 14.4 | 2.8-3.2 | 0.15 | 0.16 |
| 25 | 18 | $3.5-4$ | 0.23 | 0.25 |
| 32 | 23.2 | 4.4-5 | 0.36 | 0.42 |
| 40 | 29 | 5.5-6.2 | 0.57 | 0.66 |
| 50 | 36.2 | $6.9-7.7$ | 0.9 | 1.03 |
| 63 | 45.8 | 8.6-9.6 | 1.4 | 1.65 |
| 75 | 54.4 | 10.3-11.5 | 2 | 2.32 |
| 90 | 65.4 | 12.3-13.7 | 2.85 | 3.36 |
| 110 | 79.8 | 15.1-16.8 | 4.19 | 5 |
| 125 | 90.8 | 17.1-19 | 5.52 | 6.47 |
| 160 | 116.2 | 21.9-24.2 | 8.69 | 10. |

(1)

| S2.5 SDR6 PN20 application classes/design pressure: 5/6; 4/10; 2/8; 1/10 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Nominal diameter (mm) | Internal diameter (mm) | Thickness (mm) | Weight (kg/m) | Capacity (1/m) |
| 16 | 10.6 | 2.7-3.1 | 0.11 | 0.09 |
| 20 | 13.2 | 3.4-3.9 | 0.17 | 0.14 |
| 25 | 16.6 | 4.2-4.8 | 0.26 | 0.22 |
| 32 | 21.2 | 5.4-6.1 | 0.42 | 0.35 |
| 40 | 26.6 | 6.7-7.5 | 0.66 | 0.56 |
| 50 | 334 | 8.3-9.3 | 1.03 | 0.87 |
| 63 | 42 | 10.5-11.7 | 1.65 | 1.38 |
| 75 | 50 | 12.5-13.9 | 2.3 | 1.96 |
| 90 | 60 | 15-16.6 | 3.31 | 2.83 |
| 110 | 73.4 | 18.3-20.3 | 4.9 | 4.21 |
| 125 | 83.4 | 20.8-23 | 6.42 | 5.46 |


| Period of <br> operation |  | Pressure (mbar) |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Temp. | Years of service | S5 SDR11 single layer | S3.2 SDR7. 4 single layer | S2.5 SDR6 single layer |
| $10^{\circ} \mathrm{C}$ | 1 | 17,6 | 27,8 | 35 |
|  | 5 | 16,6 | 26,4 | 33,2 |
|  | 10 | 16,1 | 25,5 | 32,1 |
|  | 25 | 15,6 | 24,7 | 31,1 |
|  | 50 | 15,2 | 24 | 30,3 |
| $20^{\circ} \mathrm{C}$ | 1 | 15 | 23,8 | 30 |
|  | 5 | 14,1 | 22,3 | 28,1 |
|  | 10 | 13,7 | 21,7 | 27,3 |
|  | 25 | 13,3 | 21,1 | 26,5 |
|  | 50 | 12,9 | 20,4 | 25,7 |
| $30^{\circ} \mathrm{C}$ | 1 | 12,8 | 20,2 | 25,5 |
|  | 5 | 12 | 19 | 23,9 |
|  | 10 | 11,6 | 18,3 | 23,1 |
|  | 25 | 11,2 | 17,7 | 22,3 |
|  | 50 | 10,9 | 17,3 | 21,8 |
| $40^{\circ} \mathrm{C}$ | 1 | 10,8 | 17,1 | 21,5 |
|  | 5 | 10,1 | 16 | 20,2 |
|  | 10 | 9,8 | 15,6 | 19,6 |
|  | 25 | 9,4 | 15 | 18,8 |
|  | 50 | 9,2 | 14,5 | 18,3 |
| $50^{\circ} \mathrm{C}$ | 1 | 9,2 | 14,5 | 18,3 |
|  | 5 | 8,5 | 13,5 | 17 |
|  | 10 | 8,2 | 13,1 | 16,5 |
|  | 25 | 8 | 12,6 | 15,9 |
|  | 50 | 7,7 | 12,2 | 15,4 |
| $60^{\circ} \mathrm{C}$ | 1 | 7,7 | 12,2 | 15,4 |
|  | 5 | 7,2 | 11,5 | 14,3 |
|  | 10 | 6,9 | 11 | 13,8 |
|  | 25 | 6,7 | 10,5 | 13,3 |
|  | 50 | 6,4 | 10,1 | 12,7 |
| $70^{\circ} \mathrm{C}$ | 1 | 6,5 | 10,3 | 13 |
|  | 5 | 6 | 9,5 | 11,9 |
|  | 10 | 5,9 | 9,3 | 11,7 |
|  | 25 | 5,1 | 8 | 10,1 |
|  | 50 | 4,3 | 6,7 | 8,5 |
| $80^{\circ} \mathrm{C}$ | $1$ | 5,5 | 8,6 | 10,9 |
|  | $5$ | 4,8 | 7,6 | 9,6 |
|  | 10 | 4 | 6,3 | 8 |
|  | 25 | 3,2 | 5,1 | 6,4 |
| $90^{\circ} \mathrm{C}$ | 1 | --- | 6,1 | 7,7 |
|  | 5 | --- | 4 | 5 |


| Period of operation |  | Pressure (mbar) |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Tempera |  | Years of | S3. 2 SDR7. 4 | S25 SDR6 |
| Permanent at $70^{\circ} \mathrm{C}$ with 30 days a year at | $75^{\circ} \mathrm{C}$ | 5 | 9,41 | 11,54 |
|  |  | 10 | 9,11 | 11,16 |
|  |  | 25 | 8,26 | 9,64 |
|  |  | 45 | 7,16 | 8,38 |
|  | $80^{\circ} \mathrm{C}$ | 5 | 9,1 | 11,16 |
|  |  | 10 | 8,8 | 10,8 |
|  |  | 25 | 7,86 | 9,17 |
|  |  | 42,5 | 6,9 | 8,08 |
|  | $85^{\circ} \mathrm{C}$ | 5 | 8,49 | 10,44 |
|  |  | 10 | 8,21 | 10,08 |
|  |  | 25 | 7,19 | 8,4 |
|  |  | 37,5 | 6,52 | 7,63 |
|  | $90^{\circ} \mathrm{C}$ | 5 | 7,8 | 9,6 |
|  |  | 10 | 7,5 | 9,27 |
|  |  | 25 | 6,33 | 7,4 |
|  |  | 35 | 5,83 | 6,83 |
| Permanent at $70^{\circ} \mathrm{C}$ with 60 days a year a | $75^{\circ} \mathrm{C}$ | 5 | 9,36 | 11,47 |
|  |  | 10 | 9,06 | 11,1 |
|  |  | 25 | 8,1 | 9,45 |
|  |  | 45 | 7,02 | 8,22 |
|  | $8^{\circ} \mathrm{C}$ | 5 | 8,9 | 10,92 |
|  |  | 10 | 8,61 | 10,56 |
|  |  | 25 | 7,43 | 8,68 |
|  |  | 40 | 6,63 | 7,77 |
|  | $85^{\circ} \mathrm{C}$ | 5 | 8,23 | 10,11 |
|  |  | 10 | 7,95 | 9,77 |
|  |  | 25 | 6,54 | 7,65 |
|  |  | 35 | 6,03 | 7,06 |
|  | $90^{\circ} \mathrm{C}$ | 5 | 7,53 | 9,27 |
|  |  | 10 | 7,27 | 8,95 |
|  |  | 25 | 5,57 | 6,53 |
|  |  | 30 | 5,33 | 6,25 |
| Permanent at $70^{\circ} \mathrm{C}$ with 90 days a year at | $75^{\circ} \mathrm{C}$ | 5 | 9,31 | 11,42 |
|  |  | 10 | 9,01 | 11,05 |
|  |  | 25 | 7,95 | 9,29 |
|  |  | 45 | 6,89 | 8,08 |
|  | $8^{\circ} \mathrm{C}$ | 5 | 8,77 | 10,76 |
|  |  | 10 | 8,48 | 10,41 |
|  |  | 25 | 7,11 | 8,31 |
|  |  | 37,5 | 6,44 | 7,23 |
|  | $85^{\circ} \mathrm{C}$ | 5 | 8,07 | 9,92 |
|  |  | 10 | 7,8 | 9,58 |
|  |  | 25 | 6,11 | 7,15 |
|  |  | 32,5 | 5,73 | 6,72 |
|  | $90^{\circ} \mathrm{C}$ | 5 | 7,38 | 9,08 |
|  |  | 10 | 7,13 | 8,77 |
|  |  | 25 | 5,12 | 6,01 |

### 5.2 THREE-LAYER FASER PIPES ACCORDING TO


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| FASER-CT S4 SDR 9 application classes / design pressure: 5/4; 4/8; 2/4; 1/6 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal diameter (mm) | Inemal diameter (mm) | Thidness (mm) | Layer thidnese $\mathrm{Fv}(\mathrm{mm})$ | Weight (kgm) | Capaity (1m) |
| 32 | 24,8 | 3,6-4,1 | $>0,9$ | 0,328 | 0,483 |
| 40 | 31 | 4,5-5,1 | > 1,12 | 0,511 | 0,754 |
| 50 | 38,8 | 5,6-6,3 | > 1,4 | 0,791 | 1,182 |
| 63 | 48,8 | 7,1-8 | > 1,77 | 1,261 | 1,869 |
| 75 | 58,2 | 8,4-9,4 | >2,1 | 1,771 | 2,659 |
| 90 | 69,8 | 10,1-11,3 | >2,52 | 2553 | 3,825 |
| 110 | 88,4 | 12,3-13,7 | >3,07 | 3,789 | 5,725 |
| 125 | 97 | 14-15,5 | >3,5 | 4,886 | 7,386 |
| 160 | 124,2 | 17,9-19,8 | >4,47 | 7,987 | 12,109 |


| FASER S3.2 SDR7.4 application classes/design pressure: 5/6; 4/10; 2/6; 1/8 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal diamater (mm) | Inemal diamter (mm) | Thichnes (mm) | Layer tididness FV (mm) | Weight (kytm) | Capaity (lm) |
| 20 | 14.4 | 2.8-3.2 | > 0.7 | 0.16 | 0.16 |
| 25 | 18 | $3.5-4$ | > 0.9 | 0.25 | 0.25 |
| 32 | 23.2 | 4.4 - 5 | > 1.1 | 0.39 | 0.42 |
| 40 | 29 | 5.5-6.2 | > 1.4 | 0.61 | 0.66 |
| 50 | 36.2 | $6.9-7.7$ | > 1.8 | 0.95 | 1.03 |
| 63 | 45.8 | 8.6-9.6 | >2.2 | 1.49 | 1.65 |
| 75 | 54.4 | 10.3-11.5 | >2.6 | 2.11 | 2.32 |
| 90 | 65.4 | 12.3-13.7 | > 3.07 | 3.03 | 3.36 |
| 110 | 79.8 | 15.1-16.8 | > 3.77 | 4.53 | 5 |
| 125 | 90.8 | 17.1-19 | > 4.26 | 6.21 | 6.47 |
| 160 | 116.2 | 21.9-24.2 | > 5.47 | 9.75 | 10.6 |


| Period of operation |  |  | Pressure (bar) |  |  | $10^{\circ} \mathrm{C}$ | 10 | $\begin{aligned} & 26,2 \\ & 25,6 \end{aligned}$ | $\begin{aligned} & 27,9 \\ & 27,5 \end{aligned}$ | $\begin{aligned} & 28,2 \\ & 27,7 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |
| Temperature |  | Years of service | S5 SDR11 Faser Climate | S4 SDR9 Repolen Faser | S3,2 SDR7,4 <br> Repolen Faser |  | 25 | 24,7 | 27,1 | 26,9 |
|  | $75^{\circ} \mathrm{C}$ | 5 | 9,38 | 12,9 | 14,27 |  | 50 | 24,1 | 26,7 | 26,1 |
|  |  | 10 | 9,08 | 12,6 | 13,79 |  | 100 | 23,5 | 26,3 | 25,2 |
|  |  | 25 | 7,82 | 12,2 | 11,74 | ${ }^{15}{ }^{\circ} \mathrm{C}$ | 1 | 25,7 | 26,9 | 29,4 |
|  |  | 45 | 6,77 | 12,2 12 | 10,18 |  | 5 | 24,2 | 26 | 27,4 |
|  | $80^{\circ} \mathrm{C}$ | 5 | 8,88 | 11,7 | 13,5 |  | 10 | 23,6 | 25,7 | 26,9 |
|  |  | 10 | 8,46 | 11,4 | 12,8 |  | 25 | 22,8 | 25,2 | 26,1 |
|  |  | 25 | 7,38 | 11,1 | 11,14 |  | 50 | 22,2 | 24,9 | 25,3 |
|  |  | 42,5 | 6,49 | 10,9 | 9,79 |  | 100 | 21,6 | 24,5 | 24,5 |
|  | $8^{\circ} \mathrm{C}$ |  |  |  |  | $20^{\circ} \mathrm{C}$ | 1 | 23,8 | 25 | 28,6 |
|  |  | 5 | 8,17 | 10,7 | 12,42 |  | 5 | 22,3 | 24,2 | 26,8 |
|  |  | 10 | 7,82 | 10,4 | 11,87 |  | 10 | 21,7 | 23,9 | 26,1 |
|  |  | 25 | 6,7 | 10,1 | 10,14 |  | 25 | 21 | 23,5 | 25,3 |
|  |  | 37,5 | 6,07 | 10 | 9,18 |  | 50 | 20,4 | 23,1 | 24,5 |
|  | $90^{\circ} \mathrm{C}$ | 5 | 7,5 | 9,8 | 11,39 |  | 100 | 19,9 | 22,8 | 23,7 |
|  |  | 10 | 7,19 | 9,5 | 10,94 | $30^{\circ} \mathrm{C}$ | 1 | 20,2 | 21,7 | 24,3 |
|  |  | 25 | 5,85 | 9,2 | 8,86 |  | 5 | 18,9 | 20,9 | 22,8 |
|  |  | 35 | 5,39 | 9,1 | 8,16 |  | 10 | 18,4 | 20,6 | 22 |
| Permanent at <br> $70^{\circ} \mathrm{C}$ with 60 days a year a | $75^{\circ} \mathrm{C}$ | 5 | 9,26 | 12,3 | 14,11 |  | 25 | 17,8 | 20,2 | 21,3 |
|  |  | 10 | 8,9 | 12,1 | 13,57 |  | 25 50 | 17,8 | 20,2 | 20, |
|  |  | 25 | 7,62 | 11,7 | 11,58 |  | 50 |  |  | 20,7 |
|  |  | 45 | 6,6 | 11,5 | 10,05 |  | 100 | 6,8 | 19,7 | 20 |
|  | $80^{\circ} \mathrm{C}$ | 5 | 8,61 | 11,4 | 13,12 | $40^{\circ} \mathrm{C}$ | 1 | 17,1 | 18,6 | 20,5 |
|  |  | 10 | 8,24 | 11,2 | 12,54 |  | 5 | 16 | 18 | 19,2 |
|  |  | 25 | 6,93 | 10,8 | 10,56 |  | 10 | 15,6 | 17,7 | 18,7 |
|  |  | 40 | 6,18 | 10,7 | 9,41 |  | 25 | 15 | 17,3 | 18 |
|  | $85^{\circ} \mathrm{C}$ | 5 | 7,91 | 10,4 | 12,03 |  | 50 | 14,6 | 17,1 | 17,5 |
|  |  | 10 | 7,56 | 10,2 | 11,52 |  | 100 | 14,1 | 16,8 | 16,8 |
|  |  | 25 | 6,05 | 9,9 | 9,22 | $5^{50} \mathrm{C}$ | 1 | 14,5 | 15,9 | 17,5 |
|  |  | 35 | 5,57 | 9,8 | 8,48 |  | 5 | 13,5 | 15,3 | 16,2 |
|  | $90^{\circ} \mathrm{C}$ | 5 | 7,25 | 9,5 | 11,04 |  | 10 | 13,1 | 15,1 | 15,7 |
|  |  | 10 | 6,4 | 9,3 | 9,76 |  | 25 | 12,6 | 14,7 | 15,2 |
|  |  | 25 | 5,12 | 9,1 | 7,81 |  | 50 | 12,2 | 14,5 | 14,7 |
| Permanentat <br> $70^{0} \mathrm{C}$ with 90 <br> days a year a | $75^{\circ} \mathrm{C}$ | 30 5 | 4,9 | 12,2 | 7,46 |  | 100 | 11,9 | 14,3 | 14,1 |
|  |  | 10 | 8,79 | 12 | 13,38 |  | 1 | 12,2 | 13,5 | 14,7 |
|  |  | 25 | 7,45 | 11,6 | 11,33 |  | 5 | 11,4 | 13 | 13,7 |
|  |  | 45 | 6,45 | 11,4 | 9,82 | $60^{\circ} \mathrm{C}$ | 10 | 11 | 12,7 | 13,2 |
|  | $80^{\circ} \mathrm{C}$ | 5 | 8,46 | 11,3 | 12,9 |  | 25 | 10,6 | 12,4 | 12,6 |
|  |  | 10 | 8,11 | 11 | 12,35 |  | 50 | 10,3 | 12,2 | 12,1 |
|  |  | 25 | 6,6 | 10,7 | 10,05 | $70^{\circ} \mathrm{C}$ | 1 | 10,3 | 11,3 | 12,4 |
|  |  | 37,5 | 5,98 | 10,6 | 9,09 |  | 5 | 9,6 | 10,9 | 11,4 |
|  | $8^{5}{ }^{\circ} \mathrm{C}$ | 5 | 7,76 | 10,3 | 11,81 |  | 10 | 9,2 | 10,7 | 11,1 |
|  |  | 10 | 7,03 | 10,1 | 10,72 |  | 25 | 8 | 10,4 | 9,6 |
|  |  | 25 | 5,63 | 9,8 | 8,58 |  | ${ }_{5}$ | 8 | 10,4 | 9,6 |
|  |  | 32,5 | 5,28 | 9,7 | 8,03 |  | 50 | 6,8 | 10,2 | 8,1 |
|  | $90^{\circ} \mathrm{C}$ | 5 | 6,96 | 9,4 | 10,59 | $75^{\circ} \mathrm{C}$ | ${ }^{1}$ | 9,4 | 10,4 | 11,7 |
|  |  | 10 | 5,88 | 9,2 | 8,96 |  | 5 | 8,7 | 9,9 | 10,8 |
|  |  | 25 | 4,7 | 8,9 | 7,17 |  | 10 | 8 | 9,7 | 10 |
|  |  |  |  |  |  |  | 25 | 6,4 | 9,5 | 8 |
|  |  |  |  |  |  |  | 50 | 5,4 | 9,3 | 6,7 |
|  |  |  |  |  |  | ${ }^{80}{ }^{\circ} \mathrm{C}$ | 1 | 8,6 | 9,5 | 10,4 |
|  |  |  |  |  |  |  | 5 | 7,7 | 9 | 9,2 |
|  |  |  |  |  |  |  | 10 | 6,5 | 8,9 | 7,8 |
|  |  |  |  |  |  |  | 25 | 5,2 | 8,6 | 6,2 |
|  |  |  |  |  |  | $90^{\circ} \mathrm{C}$ | 1 | 7,2 | 7,8 | 8,7 |
|  |  |  |  |  |  |  | 5 | 5,1 | 7,4 | 6 |
|  |  |  |  |  |  |  | 10 | 4,3 | 7,3 | 5,1 |

### 5.3 FITTINGS

TERMO FUSION



SYSTEM
FEATURES
6.1 Main advantages
$\begin{array}{ll}\text { 6.2 } & \text { Application fields } \\ \text { 6.3 } & \text { Marking and traceability }\end{array}$
6.3 Marking and traceability
6.4 Handling and storage
6.4 Handling and storage
$\begin{array}{ll}\text { 6.5 } & \text { Antilegionella treatments } \\ \text { 6.6 } & \text { Recycling-Environment }\end{array}$

### 6.1 MAIN ADVANTAGES

- High resistance to long-term internal pressure and high tem peratures.
$\square$ Non-toxic. Suitable for the use with drinking water. Does not add odour, colour or taste of any kind, making it especially suitable for the transport of large quantities of food products, 100 \% recyclable.
- High resistance to chemical corrosion of both acids and alkalis. Fully reliable in saline environments (sea water, etc.)
$\square$ Interior with mirror finish, which means total absence of fouling and very low pressure drop.
$\square$ Low thermal conductivity coefficient. Low heat loss. Minimal condensation.Electrical insulator. High resistance to eddy currents.


### 6.2 APPLICATION FIELDS

REPOLEN systems are designed to provide solutions in all those applications that require the transport of pressurised cold and hot water, both for human consumption and domestic or industrial use.
In addition to its basic applications, the system's great features make it possible for it to be used in endlessly different applications.
The great difference between the REPOLEN and the REPOLEN FASER systems lies in the difference in lineal expansion, which makes it possible for it to adapt to the possibilities of each installation.
Some of the most common uses are:


Hydrosanitary installations: Connections, meters and mani-
fold panels, pillars, distribution branches, boilers, accumulators, return lines.

Very easy to assemble. Much lighter than other traditional ma terials.

- Highly resistant to abrasion.

Excellent behaviour to antilegionella treatments according to standard.

- Very low noise transmission level.

Very low celerity (wave propagation velocity).
Resistant to cold. Given the material's plasticity, it is capable of absorbing most of the volume increase in cases of freezing.

- Acoustic insulation. Thanks to the low celerity of the material (wave propagation velocity), it features an excellent damping effect against the transmission of noise during fluids' passage.


Air conditioning both with fan coils and radiant floor


Heating in even high-temperatu-
re boilers, radiant floor, radiators, re boile
etc.


Thermal waters, swimming pools, geothermal installations


Facilities sensitive to disinfection against legionella, such as hospitals, schools, institutional buildings, hotels, sports facilities, etc.


Recycled water installation where even solids may be washed away.


Compressed air systems.

Installations for the transport of industrial liquids: industrial refrigeration, chemical industries, food industries, ...

Pipes marking is done in accordance with the UNE EN ISO 15874 standard and the requirements of the AENOR Special Regulations, RP.001.52, and RP.001.72. The purpose of pipe marking is to provide the necessary information to the installer, the user and the manufacturer, if necessary. The marking includes:

## - Trademark: REPOLEN

Reference to the AENOR mark (Product Certificate or Certificate of Conformity) and contract number

- Material it is made of

Nominal diameter and thickness

- Application class and nominal pressure (see below)

Manufacturing period

- Reference standard
- Symbol for suitability for food use

Reference to $100 \%$ ntionl mane

The manufacturing period is unique for each pipe production, enabling complete traceability of the finished product. Knowing this number makes it possible to make a complete tracking, from the entry of raw material to the delivery at our clients' home

As for the application class, according to the standard, pipes are marked with the design pressure (not nominal or working pressure) for a given application class. The design pressure is defined as the maximum pressure in relation to the circumstances for which the system has been designed.
 According to the standard, these pressures are $4,6,8$ and 10 bar

With regard to the application class, the standard distinguishes between 4 classes:

| $\begin{aligned} & \text { Application } \\ & \text { class } \end{aligned}$ | Design temperature ( $\left.{ }^{\circ} \mathrm{C}\right)$ DT | Time to DT (years) | $\begin{gathered} \text { Maximum } \\ \text { temperature } \\ \left({ }^{\circ} \mathrm{C}\right) \text { Tmax } \end{gathered}$ | $\begin{gathered} \text { Time to } \\ \substack{\text { Timax } \\ \text { (years) }} \end{gathered}$ | $\begin{gathered} \text { Malfunctioning } \\ \text { temperature Tmal } \\ \left({ }^{\circ} \mathrm{C}\right) \end{gathered}$ | Time to Tma (years) | Typical field of application |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 60 | 49 | 80 | 1 | 95 | 100 | Hot water supply ( $60^{\circ} \mathrm{C}$ ) |
| 2 | 70 | 49 | 80 | 1 | 95 | 100 | Hot water supply ( $70^{\circ} \mathrm{C}$ ) |
| 4 | $\begin{gathered} 20 \\ \text { followed by } 40 \\ \text { followed by } 60 \end{gathered}$ | $\begin{aligned} & 2.5 \\ & 20 \\ & 25 \end{aligned}$ | 70 | 2.5 | 100 | 100 | Heating by radiant floor and low-temperature radiators |
| 5 | $\begin{aligned} & 20 \\ & \text { followed by } 40 \\ & \text { followed by } 80 \end{aligned}$ | $\begin{aligned} & 14 \\ & 25 \\ & 10 \end{aligned}$ | 90 | 1 | 100 | 100 | High temperature radiators |

However, in order to facilitate the use of the pipes, they are also marked with the theoretical nominal pressure if they were to work at $20^{\circ} \mathrm{C}$ for 50 years.
Even if it is not marked on the pipe, it is advisable to know the SDR and the S:

- SDR is the relation between the outer diameter and the thickness of the pipe, according to the equation:


## $\mathrm{SDR}=\varphi$ ext $/$ thickness

Sis a dimensionless number that classifies the piping according to ISO 4065 standard and indicates the relationship between the tangential tension $(\sigma)$ and the working pressure $(P)$ at a given temperature, according to:

### 6.4 HANDLING AND STORAGE

- Resistance to ultraviolet rays (UV)

PPR should not be exposed to solar radiation. Even when stabilised against this radiation, its continuous exposure causes material degradation, thus accelerating its ageing.

Resistance to low temperatures
At temperatures below $0^{\circ} \mathrm{C}$, PPR, being a crystalline material, becomes fragile. It is therefore important, especially during transport and handling, to avoid any kind of impact. However, once installed, its plasticity is capable of absorbing volume variations due to the freezing of the liquids flowing inside.

## $\square$ Arrangement of the pipes

It is important to try to ensure that the pipes are always horizontal and to try to avoid, as far as possible, their curvature in order to prevent deformations that make subsequent installation difficult.


## $\square$ Bending

Thanks to the plasticity of the pipes, they allow a certain curvature. The maximum radius of curvature is 8 times its diameter. If bending is necessary, hot air heaters can be used, never direct torch, as this could destroy the molecular structure of the pipe.

## $\square$ Threading

Conical plugs should be avoided in the female threaded terminals, as they could deteriorate the threads. Teflon or similar can be used in appropriate quantities to ensure tightness.

## ANTILEGIONELLA TREATMENTS 6.5

Due to their characteristics, Repolen piping do not favour the cultivation of any type of microorganism or known bacteria. However, in cases where disinfection is required, Repolen pipes do not present any problems as long as the disinfection is carried out in accordance with current standards.

In accordance with the current standards, for the control and prevention of Legionella (UNE 100030) and with Royal Decree RD863/2003, the following disinfection methods are recommended:

- Chemical use in reservoirs

For cold water for human consumption, maximum concentrations of 20 to 30 ppm of free residual chlorine for a maximum of between 3 and 1 hour respectively for water at pH 7 inside the reservoirs.

- Chemical use in pipings

Disinfection with $50 \mathrm{mg} / \mathrm{l}$ of free chlorine for more than 12 hours can be carried out twice a year, or $150 \mathrm{mg} / \mathrm{l}$ of oxygen peroxide can be used for 24 hours; in both cases, the temperature should never exceed $30^{\circ} \mathrm{C}$.

- Thermal way

For domestic hot water (hot water system). $70^{\circ} \mathrm{C}$ or more for 2 hours
It is very important to note that the two methods should never be used together (the combination of high temperatures with high concentrations of
chlorine can damage installations)
In some places chlorine dioxide is widely used as a disinfectant, due to its low price and its high disinfectant effect. However, its use is not recommended since its high oxidation potential may eventually affect the installations (metallic or plastic).

## RECYCLING - ENVIRONMENT 6.6



PPR REPOLEN's piping are made of $100 \%$ virgin materials (the standards do not authorise the use of recycled materials for drinking water) and they are also $100 \%$ recyclable.

They are also environmentally friendly materials since their contamination is purely visual.



INSTALLATION


### 7.1 EXPANSION CALCULATION

REPOLEN PP-R and PPR FASER pipings are subject to thermal expansion in exactly the same way as other construction materials. This makes it necessary to compensate for this lineal expansion when calculating the installation. Built-in piping absorbs this lineal expansion towards the inside.

There are several formulas according to ENV 12108. The calculation equation is as follows:
$\Delta \mathrm{L}=\mathrm{L} * \lambda * \Delta \mathrm{~T}$
where: $\Delta L$ is the increase in length of the pipe due to the effect of lineal expansion, in millimetres
L is the length of the pipe on which the lineal expansion is calculated, in metres
$\lambda$ is the lineal expansion coefficient, in $\mathrm{mm} / \mathrm{m}^{\circ} \mathrm{C}$. Depends on the material
$\lambda$ PPR $=0.15 \mathrm{~mm} / \mathrm{m}^{\circ} \mathrm{C}$
$\lambda$ faser $=0.03 \mathrm{~mm} / \mathrm{m}^{\circ} \mathrm{C}$
$\Delta T$, is the temperature difference between the transported fluid and the ambient temperature


These lineal expansions are to be calculated between fixed points or changes of direction. If there is little lineal expansion and the installation can absorb it, it is best to allow mobility at the ends. If this mobility cannot be allowed and there is little lineal expansion, dilating sleeves can be used. The most common is to make bows, either in loop (if the pipe allows, it is not very frequent) or in $U$ shape.


Clamps marked as PF fix the pipe (anchoring), making its mobility not possible, while the PD, if available, only provide support (guide).

The equation used for the bow calculations is
$\mathrm{LB}=2 * \mathrm{LD}+\mathrm{LA}=\mathrm{k} * \sqrt{\mathrm{D} * \Delta \mathrm{~L}}$
where: LB is the total flexible arm
LD is the length of the transverse arm
LA is the length of the longitudinal arm $\quad \mathrm{LA}=0.5 \times \mathrm{LD}$
k is a material-specific constant, which for PPR is 20
D is the nominal diameter of the pipe

Example: A 8 m long pipe with a 25 mm diameter will be installed to transport water at $70^{\circ} \mathrm{C}$ in an environment with a temperature of $25^{\circ} \mathrm{C}$, approximately.

- Installations with single-layer PPR
$\Delta \mathrm{L}=8 * 0.15 *(70-25)=54 \mathrm{~mm}$
We'll have to compensate 54 mm
For calculating the bow:
$\mathrm{LB}=20 * \sqrt{25 * 54}=734.85 \cong 735 \mathrm{~mm}$
$\mathrm{LB}=2^{\star} \mathrm{LD}+0.5 * \mathrm{LD} \Rightarrow \mathrm{LD}={ }^{735} 2.5294 \mathrm{~mm}$
$\mathrm{LA}=294 * 0.5=147 \mathrm{~mm}$
That is, the bow will have two transversal arms of 294 mm each and one longitudinal arm of 147 mm
$\square$ Installations with PPR REPOLEN

$$
\Delta \mathrm{L}=8 * 0.03 *(70-25)=10.8 \mathrm{~mm}
$$

Well have to compensate 10.8 mm
For calculating the bow:
$\mathrm{LB}=20 \star \sqrt{25 * 10.8}=328.63 \cong 329 \mathrm{~mm}$
$\mathrm{LB}=2 * \mathrm{LD}+0.5 * \mathrm{LD} \Rightarrow \mathrm{LD}={ }^{329}{ }_{2 . \overline{5}}$
$=131.6 \cong 132 \mathrm{~mm}$

## $\mathrm{LA}=132 * 0.5=66 \mathrm{~mm}$

That is, the bow will have two transversal arms of 132 mm each one and one longitudinal of 66 mm

| $\lambda=0,15 \mathrm{~mm} / \mathrm{m}^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Piping } \\ \text { length }(\mathrm{m}) \end{gathered}$ | Temperature difference $\Delta$ Tee ( ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |
|  | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 |
|  | Lineal expansion of PPR REPOLEN piping $\Delta 1$ (mm) |  |  |  |  |  |  |  |
| 0,1 | 0,15 | 0,3 | 0,45 | 0,6 | 0,75 | 0,9 | 1,05 | 1,2 |
| 0,2 | 0,3 | 0,6 | 0,9 | 1,2 | 1,5 | 1,8 | 2,1 | 2,4 |
| 0,3 | 0,45 | 0,9 | 1,35 | 1,8 | 2,25 | 2,7 | 3,15 | 3,6 |
| 0,4 | 0,6 | 1,2 | 1,8 | 2,4 | 3 | 3,6 | 4,2 | 4,8 |
| 0,5 | 0,75 | 1,5 | 2,25 | 3 | 3,75 | 4,5 | 5,25 | 6 |
| 0,6 | 0,9 | 1,8 | 2,7 | 3,6 | 4,5 | 5,4 | 6,3 | 7,2 |
| 0,7 | 1,05 | 2,1 | 3,15 | 4,2 | 5,25 | 6,3 | 7,35 | 8,4 |
| 0,8 | 1,2 | 3,6 | 3,6 | 4,8 | 6 | 7,2 | 8,4 | 9,6 |
| 0,9 | 1,35 | 2,7 | 4,05 | 5,4 | 6,75 | 8,1 | 9,45 | 10,8 |
| 1 | 1,5 | 3 | 4,5 | 6 | 7,5 | 9 | 10,5 | 12 |
| 2 | 3 | 6 | 9 | 12 | 15 | 18 | 21 | 24 |
| 3 | 4,5 | 9 | 13,5 | 18 | 22,5 | 27 | 31,5 | 36 |
| 4 | 6 | 12 | 18 | 24 | 30 | 36 | 42 | 48 |
| 5 | 7,5 | 15 | 22,5 | 30 | 37,5 | 45 | 52,5 | 60 |
| 6 | 9 | 18 | 27 | 36 | 45 | 54 | 63 | 72 |
| 7 | 10,5 | 21 | 31,5 | 42 | 52,5 | 63 | 73,5 | 84 |
| 8 | 12 | 24 | 36 | 48 | 60 | 72 | 84 | 96 |
| 9 | 13,5 | 27 | 40,5 | 54 | 67,5 | 81 | 94,5 | 108 |
| 10 | 20 | 40 | 60 | 80 | 100 | 120 | 140 | 160 |


| $\begin{aligned} & \text { Piping } \\ & \text { length }(\mathrm{m}) \end{aligned}$ | $\lambda=0,03 \mathrm{~mm} / \mathrm{m}^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Temperature difference $\Delta$ Tee ( ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |
|  | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 |
|  | Lineal expansion of REPOLEN piping PPR FASER $\Delta 1$ (mm) |  |  |  |  |  |  |  |
| 0,1 | 0,03 | 0,06 | 0,09 | 0,12 | 0,15 | 0,18 | 0,21 | 0,24 |
| 0,2 | 0,06 | 0,12 | 0,18 | 0,24 | 0,3 | 0,36 | 0,42 | 0,48 |
| 0,3 | 0,09 | 0,18 | 0,27 | 0,36 | 0,45 | 0,54 | 0,63 | 0,72 |
| 0,4 | 0,12 | 0,24 | 0,36 | 0,48 | 0,6 | 0,72 | 0,84 | 0,96 |
| 0,5 | 0,15 | 0,3 | 0,45 | 0,6 | 0,75 | 0,9 | 1,05 | 1,2 |
| 0,6 | 0,18 | 0,36 | 0,54 | 0,72 | 0,9 | 1,08 | 1,26 | 1,44 |
| 0,7 | 0,21 | 0,42 | 0,63 | 0,84 | 1,05 | 1,26 | 1,47 | 1,68 |
| 0,8 | 0,24 | 0,44 | 0,72 | 0,96 | 1,2 | 1,44 | 1,68 | 1,92 |
| 0,9 | 0,27 | 0,54 | 0,81 | 1,08 | 1,35 | 1,62 | 1,89 | 2,16 |
| 1 | 0,3 | 0,6 | 0,9 | 1,2 | 1,5 | 1,8 | 2,1 | 2,4 |
| 2 | 0,6 | 1,2 | 1,8 | 2,4 | 3 | 3,6 | 4,2 | 4,8 |
| 3 | 0,9 | 1,8 | 2,7 | 3,6 | 4,5 | 5,4 | 6,3 | 7,2 |
| 4 | 1,2 | 2,4 | 3,6 | 4,8 | 6 | 7,2 | 8,4 | 9,6 |
| 5 | 1,5 | 3 | 4,5 | 6 | 7,5 | 9 | 10,5 | 12 |
| 6 | 1,8 | 3,6 | 5,4 | 7,2 | 9 | 10,8 | 12,6 | 14,4 |
| 7 | 2,1 | 4,2 | 6,3 | 8,4 | 10,5 | 12,6 | 14,7 | 16,8 |
| 8 | 2,4 | 4,8 | 7,2 | 9,6 | 12 | 14,4 | 16,8 | 19,2 |
| 9 | 2,7 | 5,4 | 8,1 | 10,8 | 13,5 | 16,2 | 18,9 | 21,6 |
| 10 | 3 | 6 | 9 | 12 | 15 | 18 | 21 | 24 |




Piping can be installed on trays or half rods, in a way that they can be used as support. As a result, when there are long sections exposed, the lineal expansions will ensure the piping movement on the tray but they will avoid the unsightly effect that lineal expansions may cause.

The recommended distances are:

| Diameter | PPR single layer |  |  |  | Three-layer FASER |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Distance for tray clamping |  | Distance for pipe tray damping |  | Distance for tey camping |  | Distance for proctey damping |  |
|  | Water $<30^{\circ} \mathrm{C}$ | Water $>30^{\circ} \mathrm{C}$ | Water $<30^{\circ} \mathrm{C}$ | Water $30^{\circ} \mathrm{C}$ | Water $<30^{\circ} \mathrm{C}$ | Water $30^{\circ} \mathrm{C}$ | Water $300^{\circ} \mathrm{C}$ | Water $300^{\circ} \mathrm{C}$ |
| 16/20 | 1500 | 1000 | 500 | 200 | 1950 | 1300 | 650 | 260 |
| 25 | 1500 | 1200 | 500 | 300 | 1950 | 1560 | 650 | 390 |
| 32 | 1500 | 1200 | 750 | 400 | 1950 | 1560 | 975 | 520 |
| 40 | 1500 | 1200 | 750 | 600 | 1950 | 1560 | 975 | 780 |
| 50/63/75 | 1500 | 1500 | 750 | 750 | 1950 | 1950 | 975 | 975 |
| 90/110/125 | 2000 | 2000 | 1000 | 1000 | 2600 | 2600 | 1300 | 1300 |
| 160 | 2500 | 2500 | 1250 | 1250 | 3250 | 3250 | 1625 | 1625 |



It is very important that a riser with branches can absorb the lineal expansions without loading tension on the branches. According to the ENV 12108 , the recommended distance between two guiding clamps or between a guiding and an anchoring clamp is:

| Outer diameter (mm) | $\mathrm{L}^{*}(\mathrm{~mm})$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | PPR single layer |  |  |  | Three-layer FASER |  |  |  |
|  | $\begin{aligned} & \text { Pipes that permit length } \\ & \text { variations } \end{aligned}$ |  | Pipes that do not permit length variations |  | $\begin{aligned} & \text { Pipes that permit length } \\ & \text { variations } \end{aligned}$ |  | Pipes that do not permit length variations |  |
|  | Cold water | Hot water | Cold water | Hot water | Cold water | Hot water | Cold water | Hot water |
| 16 | 750 | 400 | 600 | 250 | 975 | 520 | 780 | 325 |
| 20 | 800 | 500 | 700 | 300 | 1040 | 650 | 910 | 390 |
| 25 | 850 | 600 | 800 | 350 | 1105 | 780 | 1040 | 455 |
| 32 | 1000 | 650 | 900 | 400 | 1300 | 845 | 1170 | 520 |
| 40 | 1100 | 800 | 1100 | 500 | 1430 | 1040 | 1430 | 650 |
| 50 | 1250 | 1000 | 1250 | 600 | 1625 | 1300 | 1625 | 780 |
| 63 | 1400 | 1200 | 1400 | 750 | 1820 | 1560 | 1820 | 975 |
| 75 | 1500 | 1300 | 1500 | 900 | 1950 | 1690 | 1950 | 1170 |
| 90 | 1650 | 1450 | 1650 | 1100 | 2145 | 1885 | 2145 | 1430 |
| 110 | 1900 | 1600 | 1850 | 1300 | 2470 | 2080 | 2405 | 1690 |
| 125 | 2100 | 1850 | 2000 | 1400 | 2730 | 2405 | 2600 | 1820 |
| 160 | 2500 | 2300 | 2300 | 1800 | 3250 | 2990 | 2990 | 2340 |

The thermal conductivity coefficient of PPR is $0.24 \mathrm{~W} / \mathrm{mK}$. If we compare it with copper ( $384 \mathrm{~W} / \mathrm{mK}$ ) or iron ( 58 $\mathrm{W} / \mathrm{mK}$ ), we will understand that with PPR REPOLEN pipes the problem of condensation is almost non-existant.

However, according to RITE, all installations containing fluids refrigerated below room temperature or above $40^{\circ} \mathrm{C}$ must carry an insulator with a thickness (conductivity of the $0.04 \mathrm{~W} /$ mK isolator), must conform with the figures in the following tables in order to avoid condensation:

| Outer diameter ofthe pipe to be lined | Maximum temperature of the fluid ( ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Hot fuids inside the building |  |  | Hot fluids outside the building |  |  |
|  | $40<T<60$ | $60<T<100$ | $100<T<180$ | $40<T<60$ | 60<T<100 | $100<$ T < 180 |
| $\varphi<35$ | 25 | 25 | 30 | 35 | 35 | 40 |
| $35<\varphi<60$ | 30 | 30 | 40 | 40 | 40 | 50 |
| $60<\varphi<90$ | 30 | 30 | 40 | 40 | 40 | 50 |
| $90<\varphi<140$ | 30 | 40 | 50 | 40 | 50 | 60 |
| $140<\varphi$ | 35 | 40 | 50 | 45 | 50 | 60 |


| Outer diameter of the pipe to be lined (mm) | Maximum temperature of the fluid ( ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cold fuids inside the building |  |  | Cold fuids outside the building |  |  |
|  | $40<T<60$ | 60<T<100 | $100<\mathrm{T}<180$ | $10<\mathrm{T}<0$ | $0<T<10$ | $\mathrm{T}>10$ |
| $\varphi<35$ | 30 | 20 | 20 | 50 | 40 | 40 |
| $35<\varphi<60$ | 40 | 30 | 20 | 60 | 50 | 40 |
| $60<\varphi<90$ | 40 | 30 | 30 | 60 | 50 | 50 |
| $90<\varphi<140$ | 50 | 40 | 30 | 70 | 60 | 50 |
| $140<\varphi$ | 50 | 40 | 30 | 70 | 60 | 50 |

If piping networks operation is continuous through the whole year, 5 mm must be added to the insulation thicknesses indicated in the tables.

For pipes with an outer diameter equal or less than 20 mm and a length of less than 5 m , from their connection to the general up to the terminal, which are embedded in partitions or floors, or within internal conduits, the insulation thickness should reach 10 mm .

If insulators with a different thermal conductivity than that given as a reference are used, the thickness is calculated using the following equation:

$$
\mathrm{d}=1_{2} *\left\{\mathrm{e}^{\text {Mrefe }^{\ln } \mathrm{d}+2, \text { dref } / \mathrm{D}}-1\right\}
$$

where: d is the thickness of the new insulator
D is the outer diameter of the pipe to be lined
$\lambda$ is the thermal conductivity of the new insulator $(\mathrm{W} / \mathrm{mK})$
$\lambda$ ref is the thermal conductivity of the insulator for which the tables were calculated ( $0.04 \mathrm{~W} / \mathrm{mK}$ )
dref is the thickness given by the tables for the referenced insulating material

Example: You want to line a pipe with a 75 mm diameter that will run inside a building that will carry water at a temperature of $80^{\circ} \mathrm{C}$, and you would like to use an insulator with a thermal conductivity of $0.037 \mathrm{~W} / \mathrm{mK}$ :
$\mathrm{D}=75 \mathrm{~mm}$
$\lambda=0.037 \mathrm{~W} / \mathrm{mK}$ $\lambda$ ref $=0.04 \mathrm{~W} / \mathrm{mK}$

According to the table, if we match row $60<\mathrm{D}<90$ with column $60<\mathrm{T}<100$, dref $=30 \mathrm{~mm}$

$$
\mathrm{d}=75 / 2 *\left\{\mathrm{e}^{0.037 / 0.04 * \ln 75+2.30 / 75}-1\right\}=27.1 \mathrm{~mm}
$$

### 7.4 START UP HYDRAULIC TEST

## WATER HAMMER

When a liquid is flowing through a piping at a constant speed and at a given time any element on the installation is operated (a valve is closed or opened, variation of a pump's speed, etc) an overpressure is caused, resulting in an unbalance in the fluidity speed of the liquid that alters flows and pressures in the different points of the pipeline. This overpressure is called water hammer and must be added to the working or service pressure.

Pressure and flow rate variations that result in a water hammer spread throughout the liquid mass in a wave-like motion. Wave propagation velocity is called celerity and is according to the water modulus of elasticity whose value varies according to the temperature and modulus of elasticity of the piping material.

The lower the value of the modulus of elasticity of the piping material, the lower the celerity and the overpressure value that can take place in the piping. It is therefore advisable to use polyethylene piping, due to their low modulus of elasticity, so as in the same operating conditions, they result in pressures that are much lower than those that would be produced with the use of classic materials, which are considerably more rigid.

Calculation of the overpressure by water hammer can be done using Michaud's equation:

$$
\Delta \mathrm{H}= \pm \frac{2 \star \mathrm{~L} * \mathrm{~V}}{\mathrm{~g} * \mathrm{~T}}
$$

for
$T>\frac{2 \star L}{a}$

If: $\Delta \mathrm{F}=$ increase of pressure or height, or water hammer (overpressure in m.w.c.)
$a=$ wave propagation velocity or celerity in $m / s$
$=$ water velocity in a constant speed of $\mathrm{m} / \mathrm{s}$
$L=$ piping length in $m$
$\mathrm{g}=$ acceleration of gravity in $\mathrm{m} / \mathrm{s}^{2}$
$\mathrm{T}=$ stopping manoeuvre time in s

The celerity is calculated with the equation:
$a=\frac{9900}{\sqrt{48.3+K_{c} * D_{m} / e}}$

$$
\mathrm{K}_{\mathrm{c}}=\frac{10^{10}}{\mathrm{E}}
$$

If: $\mathrm{Kc}=$ dimensionless indicator
$\mathrm{E}=$ piping modulus of elasticity in $\mathrm{kg} / \mathrm{m}^{2}\left(10^{8}\right.$ for PE$)$
In the case of very long pipelines, the water hammer does not reach its maximum value at the closing end (or point of change of direction), but at a generic point inside the pipe. In this case the Allievi equation is used:

$$
\Delta \mathrm{H}= \pm \frac{\mathrm{a}{ }_{\star} \mathrm{v}}{\mathrm{~g}}
$$

if
$\mathrm{T}<\frac{2{ }_{\star} \mathrm{L}}{\mathrm{a}}$

The water hammer can be mitigated in different ways

- Check valves. They are installed in the impulsions to protect in group of pumping and the emptying of the piping through the pump. They can also be placed on the pipeline operating pressure.
Flywheel. Or pumping group stop delayer. By means of a flywheel attached to the motor shaft.
- Air tank. A tank attached to the piping in which there is water and air under pressure. This air absorbs the pressure variations in the
pipeline. Requires maintenance as air dissolves in water over time. - Surge tank. A vertical tank attached to the piping and higher than the equivalent pressure the piping can withstand.
Air release valves. Prevents cavitation at high points in the installation.
- Safety valves. If there is a possibility of cavitation leading to strong overpressure.


### 7.6 PRESSURE DROP

REPOLEN piping have significantly lower pressure drops than piping made of other materials, such as copper thanks to its very low roughness coefficient, 0.007 for PPR, 0.011 for clean copper, 0.025 for clean brass. It should be considered that plastic materials do not rust, no foulings are produced, so that the roughness of the pipe virtually does not vary (depending on the use given to the pipe, fluid transported, disinfection treatments, etc.). For example, iron piping start from a roughness of 0.25 , which over time can even reach 4 .

Pressure drops in installations are due to the rubbing of the liquid against the walls of the pipe and to those coming from obstacles in the installation (tees, elbows, reducers, branches, etc)

The pressure drops of REPOLEN pipes with a water temperature of $10^{\circ} \mathrm{C}$ are indicated in the following tables. At higher temperatures, losses are slightly lower.

REPOLEN SDR 6
The first value corresponds to the pressure drop in $\mathrm{mm} / \mathrm{m}$.w.c. and the second to the average speed in $\mathrm{m} / \mathrm{s}$.

| Flow rate |  | 162.7 | $20 \times 3.4$ | 25x4.2 | 3225.4 | $\varphi$ - REPOLEN SDR 6 |  |  | 75x12.5 | $90 \times 15$ | 100x18.4 | ${ }^{125250.8}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| y/s | kgh |  |  |  |  | 40667 | $50 \times 84$ | ${ }_{63 \times 10} 5$ |  |  |  |  |
| 0.02 | 70 | 10 | 2 | 0.9 |  |  |  |  |  |  |  |  |
|  |  | 0.22 | 0.14 | 0.09 |  |  |  |  |  |  |  |  |
| 0.04 | 140 | 33 | 8 | 3 | 1 |  |  |  |  |  |  |  |
|  |  | 0.44 | 0.29 | 0.18 | 0.11 |  |  |  |  |  |  |  |
| 0.05 | 180 | 52 | 13 | 4 | 2 |  |  |  |  |  |  |  |
|  |  | 0.57 | 0.37 | 0.23 | 0.14 |  |  |  |  |  |  |  |
| 0.06 | 220 | 73 | 19 | 6 | 2 |  |  |  |  |  |  |  |
|  |  | 0.7 | 0.45 | 0.28 | 0.17 |  |  |  |  |  |  |  |
| 0.08 | 290 | 118 | 30 | 10 | 4 | 1.5 | 0.5 |  |  |  |  |  |
|  |  | 0.92 | 0.59 | 0.37 | 0.23 | 0.15 | 0.09 |  |  |  |  |  |
| 0.1 | 360 | 164 | 42 | 15 | 6 | 2 | 0.7 |  |  |  |  |  |
|  |  | 1.11 | 0.71 | 0.45 | 0.28 | 0.18 | 0.11 |  |  |  |  |  |
| 0.12 | 430 | 234 | 61 | 21 | 8 | 3 | 1.07 | 0.33 |  |  |  |  |
|  |  | 1.36 | 0.88 | 0.55 | 0.34 | 0.22 | 0.14 | 0.09 |  |  |  |  |
| 0.14 | 510 |  | 83 | 29 | 11 | 4 | 1.44 | 0.45 |  |  |  |  |
|  |  |  | 1.04 | 0.66 | 0.4 | 0.26 | 0.16 | 0.1 |  |  |  |  |
| 0.16 | 580 |  | 104 | 37 | 14 | 5 | 1.8 | 0.56 |  |  |  |  |
|  |  |  | 1.18 | 0.75 | 0.46 | 0.29 | 0.19 | 0.12 |  |  |  |  |
| 0.18 | 655 |  | 129 | 45 | 18 | 6 | 2.02 | 0.7 |  |  |  |  |
|  |  |  | 1.34 | 0.84 | 0.52 | 0.33 | 0.21 | 0.13 |  |  |  |  |
| 0.2 | 730 |  | 156 | 55 | 22 | 7.5 | 2.69 | 0.84 |  |  |  |  |
|  |  |  | 1.49 | 0.94 | 0.58 | 0.37 | 0.24 | 0.15 |  |  |  |  |
| 0.23 | 830 |  | 290 | 69 | 27 | 9 | 3.3 | 1 |  |  |  |  |
|  |  |  | 1.65 | 1.07 | 0.66 | 0.42 | 0.27 | 0.17 |  |  |  |  |
| 0.25 | 900 |  | 353 | 85 | 33 | 11 | 4.1 | 1.3 |  |  |  |  |
|  |  |  | 1.83 | 1.2 | 0.74 | 0.47 | 0.3 | 0.19 |  |  |  |  |


| Flow rate |  | $\varphi$ - REPOLEN SDR 6 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/s | kg/h | 1627 | $20 \times 3.4$ | 254.2 | 32554 | $40 \times 67$ | 50x8.4 | $63 \times 10.5$ | 75812.5 | $99 \times 15$ | $110 \times 18.4$ | 125520.8 |
| 0.3 | 1080 |  |  | 110 | 43 | 15 | 5.3 | 1.6 |  |  |  |  |
|  |  |  |  | 1.39 | 0.85 | 0.54 | 0.35 | 0.22 |  |  |  |  |
| 0.35 | 1280 |  |  | 149 | 59 | 20 | 7.1 | 2.2 |  |  |  |  |
|  |  |  |  | 1.65 | 1.01 | 0.64 | 0.41 | 0.26 |  |  |  |  |
| 0.4 | 1430 |  |  | 270 | 71 | 24 | 8 | 2.7 |  |  |  |  |
|  |  |  |  | 1.85 | 1.13 | 0.72 | 0.46 | 0.29 |  |  |  |  |
| 0.45 | 1605 |  |  |  | 87 | 30 | 10 | 3.4 |  |  |  |  |
|  |  |  |  |  | 1.27 | 0.81 | 0.52 | 0.32 |  |  |  |  |
| 0.5 | 1805 |  |  |  | 107 | 36 | 13 | 4.2 |  |  |  |  |
|  |  |  |  |  | 1.43 | 0.91 | 0.58 | 0.36 |  |  |  |  |
| 0.55 | 2005 |  |  |  | 135 | 44 | 15 | 5 |  |  |  |  |
|  |  |  |  |  | 1.55 | 1.01 | 0.65 | 0.4 |  |  |  |  |
| 0.65 | 2155 |  |  |  | 172 | 50 | 17 | 5.7 |  |  |  |  |
|  |  |  |  |  | 1.7 | 1.08 | 0.69 | 0.43 |  |  |  |  |
| 0.7 | 2530 |  |  |  | 225 | 66 | 23 | 7.6 |  |  |  |  |
|  |  |  |  |  | 1.98 | 1.27 | 0.82 | 0.51 |  |  |  |  |
| 0.75 | 2705 |  |  |  |  | 74 | 26 | 8.5 |  |  |  |  |
|  |  |  |  |  |  | 1.36 | 0.87 | 0.54 |  |  |  |  |
| 0.8 | 2280 |  |  |  |  | 83 | 29 | 9.5 |  |  |  |  |
|  |  |  |  |  |  | 1.45 | 0.93 | 0.58 |  |  |  |  |
| 0.85 | 3005 |  |  |  |  | 89 | 31 | 10 |  |  |  |  |
|  |  |  |  |  |  | 1.51 | 0.97 | 0.61 |  |  |  |  |
| 0.9 | 3255 |  |  |  |  | 103 | 36 | 11 |  |  |  |  |
|  |  |  |  |  |  | 1.63 | 1.05 | 0.66 |  |  |  |  |
| 1 | 3600 |  |  |  |  | 143 | 43 | 14 | 7.9 | 2.8 |  |  |
|  |  |  |  |  |  | 1.8 | 1.16 | 0.73 | 0.5 | 0.35 |  |  |
| 1.2 | 4320 |  |  |  |  | 198 | 59 | 19 | 9.2 | 3.9 |  |  |
|  |  |  |  |  |  | 2.16 | 1.4 | 0.87 | 0.61 | 0.42 |  |  |
| 1.3 | 4680 |  |  |  |  |  | 66 | 22 | 10.6 | 4.5 |  |  |
|  |  |  |  |  |  |  | 1.49 | 0.93 | 0.66 | 0.46 |  |  |
| 1.4 | 5040 |  |  |  |  |  | 76 | 25 | 12.1 | 5.1 |  |  |
|  |  |  |  |  |  |  | 1.62 | 101 | 0.71 | 0.5 |  |  |
| 1.6 | 5760 |  |  |  |  |  | 14 | 32 | 15.3 | 6.4 |  |  |
|  |  |  |  |  |  |  | 1.85 | 1.16 | 0.81 | 0.57 |  |  |
| 1.8 | 6480 |  |  |  |  |  | 141 | 40 | 18.8 | 7.9 |  |  |
|  |  |  |  |  |  |  | 2.08 | 1.32 | 0.92 | 0.64 |  |  |
| 2 | 7200 |  |  |  |  |  | 170 | 48 | 22.7 | 9.5 | 3.7 |  |
|  |  |  |  |  |  |  | 2.31 | 1.46 | 102 | 0.71 | 0.48 |  |
| 2.2 | 7920 |  |  |  |  |  |  | 57 | 26.9 | 11.3 | 4.4 |  |
|  |  |  |  |  |  |  |  | 1.6 | 1.12 | 0.78 | 0.52 |  |
| 2.4 | 8640 |  |  |  |  |  |  | 66 | 31.4 | 13.1 | 5.1 |  |
|  |  |  |  |  |  |  |  | 1.74 | 1.22 | 0.85 | 0.57 |  |
| 2.6 | 9360 |  |  |  |  |  |  | 76 | 36.1 | 15.1 | 5.9 | 3.1 |
|  |  |  |  |  |  |  |  | 1.88 | 1.32 | 0.92 | 0.62 | 0.48 |


| Flow rate |  | $\varphi$ - REPOLEN SDR 6 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/s | kgh | 16.27 | $20 \times 3.4$ | 25x4.2 | 3225.4 | 40667 | $50 \times 84$ | $63 \times 10.5$ | $75 \times 12.5$ | $90 \times 15$ | $110 \times 18.4$ | $125 \times 20.8$ |
| 2.8 | 10080 |  |  |  |  |  |  | 87 | 41.2 | 17.3 | 6.7 | 3.6 |
|  |  |  |  |  |  |  |  | 2.02 | 1.43 | 0.99 | 0.67 | 0.51 |
| 3 | 10800 |  |  |  |  |  |  | 111.3 | 46.6 | 19.5 | 7.5 | 4.1 |
|  |  |  |  |  |  |  |  | 2.17 | 1.53 | 1.06 | 0.71 | 0.55 |
| 3.5 | 12600 |  |  |  |  |  |  | 149 | 61.4 | 25.7 | 9.9 | 5.3 |
|  |  |  |  |  |  |  |  | 2.53 | 1.78 | 1.24 | 0.83 | 0.64 |
| 4 | 14400 |  |  |  |  |  |  |  | 77.9 | 32.6 | 12.6 | 6.7 |
|  |  |  |  |  |  |  |  |  | 2.04 | 1.41 | 0.95 | 0.73 |
| 4.5 | 16200 |  |  |  |  |  |  |  | 96.2 | 40.2 | 15.5 | 8.3 |
|  |  |  |  |  |  |  |  |  | 2.29 | 1.59 | 1.07 | 0.82 |
| 5 | 18000 |  |  |  |  |  |  |  | 116.2 | 48.5 | 18.7 | 10 |
|  |  |  |  |  |  |  |  |  | 2.55 | 1.77 | 1.19 | 0.92 |
| 6 | 21600 |  |  |  |  |  |  |  | 161.1 | 67.2 | 25.9 | 13.9 |
|  |  |  |  |  |  |  |  |  | 3.06 | 2.12 | 1.43 | 1.1 |
| 7 | 25200 |  |  |  |  |  |  |  |  | 88.6 | 34.2 | 18.3 |
|  |  |  |  |  |  |  |  |  |  | 2.48 | 1.66 | 1.28 |
| 8 | 28800 |  |  |  |  |  |  |  |  | 112.7 | 43.4 | 23.2 |
|  |  |  |  |  |  |  |  |  |  | 2.83 | 1.9 | 1.46 |
| 9 | 32400 |  |  |  |  |  |  |  |  | 139.3 | 53.6 | 28.7 |
|  |  |  |  |  |  |  |  |  |  | 3.18 | 2.14 | 1.65 |
| 10 | 36000 |  |  |  |  |  |  |  |  |  | 64.8 | 34.7 |
|  |  |  |  |  |  |  |  |  |  |  | 2.38 | 1.83 |
| 11 | 39600 |  |  |  |  |  |  |  |  |  | 77 | 41.1 |
|  |  |  |  |  |  |  |  |  |  |  | 2.61 | 2.01 |
| 12 | 43200 |  |  |  |  |  |  |  |  |  | 90 | 48.1 |
|  |  |  |  |  |  |  |  |  |  |  | 2.85 | 2.2 |
| 13 | 46800 |  |  |  |  |  |  |  |  |  | 104 | 55.6 |
|  |  |  |  |  |  |  |  |  |  |  | 3.09 | 2.38 |
| 15 | 54000 |  |  |  |  |  |  |  |  |  |  | 71.9 |
|  |  |  |  |  |  |  |  |  |  |  |  | 2.75 |
| 17 | 61200 |  |  |  |  |  |  |  |  |  |  | 92.1 |
|  |  |  |  |  |  |  |  |  |  |  |  | 3.11 |


| Flow rate |  | $\varphi$ - REPOLEN SDR 7.4 |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/s | kg/h | $25 \times 3.5$ | $32 \times 4.4$ | $40 \times 5.5$ | 5086.9 | $63 \times 8.6$ | 75x10,3 | $90 \times 12.3$ | 100x15.1 | 125x17.1 | 160x21.9 |
| 0.1 | 360 | 16.9 | 5.2 |  |  |  |  |  |  |  |  |
|  |  | 0.39 | 0.24 |  |  |  |  |  |  |  |  |
| 0.15 | 540 | 33.8 | 10.21 |  |  |  |  |  |  |  |  |
|  |  | 0.59 | 0.35 |  |  |  |  |  |  |  |  |
| 0.2 | 720 | 55.4 | 16.7 |  |  |  |  |  |  |  |  |
|  |  | 0.79 | 0.47 |  |  |  |  |  |  |  |  |
| 0.25 | 864 | 81.4 | 24.5 |  |  |  |  |  |  |  |  |
|  |  | 0.98 | 0.59 |  |  |  |  |  |  |  |  |
| 0.3 | 1080 | 111.6 | 33.6 | 11.7 |  |  |  |  |  |  |  |
|  |  | 1.18 | 0.71 | 0.45 |  |  |  |  |  |  |  |
| 0.35 | 1260 | 145.9 | 43.9 | 15.3 |  |  |  |  |  |  |  |
|  |  | 1.38 | 0.83 | 0.53 |  |  |  |  |  |  |  |
| 0.4 | 1440 | 184.2 | 55.3 | 19.2 | 6.7 |  |  |  |  |  |  |
|  |  | 1.57 | 0.95 | 0.61 | 0.39 |  |  |  |  |  |  |
| 0.45 | 1620 | 226.3 | 67.9 | 23.6 | 8.3 |  |  |  |  |  |  |
|  |  | 1.77 | 1.06 | 0.68 | 0.44 |  |  |  |  |  |  |
| 0.5 | 1800 | 272.2 | 81.5 | 28.3 | 9.9 |  |  |  |  |  |  |
|  |  | 1.96 | 1.18 | 0.76 | 0.49 |  |  |  |  |  |  |
| 0.55 | 1980 | 321.7 | 96.3 | 33.4 | 11.7 |  |  |  |  |  |  |
|  |  | 2.16 | 1.3 | 0.83 | 0.53 |  |  |  |  |  |  |
| 0.6 | 2160 |  | 112.2 | 38.9 | 13.6 |  |  |  |  |  |  |
|  |  |  | 1.42 | 0.91 | 0.58 |  |  |  |  |  |  |
| 0.65 | 2340 |  | 129 | 44.7 | 15.6 | 5.2 |  |  |  |  |  |
|  |  |  | 1.54 | 0.98 | 0.63 | 0.4 |  |  |  |  |  |
| 0.7 | 2520 |  | 147 | 50.9 | 17.8 | 6 |  |  |  |  |  |
|  |  |  | 1.66 | 1.06 | 0.68 | 0.439 |  |  |  |  |  |
| 0.75 | 2700 |  | 165.9 | 57.4 | 20 | 6.7 |  |  |  |  |  |
|  |  |  | 1.77 | 1.14 | 0.73 | 0.46 |  |  |  |  |  |
| 0.8 | 2880 |  | 185.9 | 64.3 | 22.4 | 7.5 |  |  |  |  |  |
|  |  |  | 1.89 | 1.21 | 0.78 | 0.49 |  |  |  |  |  |
| 0.85 | 3060 |  | 206.8 | 71.5 | 24.9 | 8.3 |  |  |  |  |  |
|  |  |  | 2.01 | 1.29 | 0.83 | 0.52 |  |  |  |  |  |
| 0.9 | 3240 |  | 228.7 | 79.1 | 27.6 | 9.2 |  |  |  |  |  |
|  |  |  | 2.13 | 1.36 | 0.87 | 0.55 |  |  |  |  |  |
| 1 | 3600 |  |  | 95.2 | 33.1 | 11.1 | 4.9 |  |  |  |  |
|  |  |  |  | 1.51 | 0.97 | 0.61 | 0.43 |  |  |  |  |
| 1.2 | 4320 |  |  | 131.2 | 45.6 | 15.2 | 6.7 |  |  |  |  |
|  |  |  |  | 1.82 | 1.17 | 0.73 | 0.52 |  |  |  |  |
| 1.4 | 5040 |  |  | 172.3 | 59.9 | 20 | 8.8 | 3.7 |  |  |  |
|  |  |  |  | 2.12 | 1.36 | 0.86 | 0.61 | 0.42 |  |  |  |


| Flow rate |  | $\varphi$ - REPOLEN SDR 7.4 |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/s | kg/h | $25 \times 3.5$ | $32 \times 4.4$ | $40 \times 5.5$ | $50 \times 6.9$ | 6388.6 | 75x10.3 | $90 \times 12.3$ | 100x15.1 | 125x17.1 | 160x21.9 |
| 1.6 | 5760 |  |  |  | 75.8 | 25.2 | 11.1 | 4.7 |  |  |  |
|  |  |  |  |  | 1.55 | 0.98 | 0.69 | 0.48 |  |  |  |
| 1.8 | 6480 |  |  |  | 9.3 | 31.1 | 13.6 | 5.7 |  |  |  |
|  |  |  |  |  | 1.75 | 1.1 | 0.78 | 0.54 |  |  |  |
| 2 | 7200 |  |  |  | 112.5 | 20 | 16.4 | 6.9 |  |  |  |
|  |  |  |  |  | 1.94 | 1.22 | 0.87 | 0.6 |  |  |  |
| 2.2 | 7920 |  |  |  | 133.2 | 44.3 | 19.4 | 8.2 |  |  |  |
|  |  |  |  |  | 2.14 | 1.35 | 0.95 | 0.66 |  |  |  |
| 2.4 | 8640 |  |  |  |  | 51.6 | 22.7 | 9.05 |  |  |  |
|  |  |  |  |  |  | 1.47 | 1.04 | 0.72 |  |  |  |
| 2.6 | 9360 |  |  |  |  | 69.5 | 26.1 | 11 |  |  |  |
|  |  |  |  |  |  | 1.59 | 1.13 | 0.78 |  |  |  |
| 2.8 | 10080 |  |  |  |  | 67.9 | 29.8 | 12.5 | 4.6 |  |  |
|  |  |  |  |  |  | 1.71 | 1.21 | 0.84 | 0.56 |  |  |
| 3 | 10800 |  |  |  |  | 76.7 | 33.6 | 14.1 | 5.4 | 2.9 |  |
|  |  |  |  |  |  | 1.84 | 1.3 | 0.9 | 0.6 | 0.46 |  |
| 3.5 | 12600 |  |  |  |  | 100.9 | 44.2 | 18.6 | 7.1 | 3.8 |  |
|  |  |  |  |  |  | 21.4 | 1.52 | 1.05 | 0.7 | 0.54 |  |
| 4 | 14400 |  |  |  |  | 128 | 56 | 23.5 | 8.9 | 4.8 |  |
|  |  |  |  |  |  | 2.45 | 1.73 | 1.21 | 0.8 | 0.62 |  |
| 4.5 | 16200 |  |  |  |  | 158 | 69.1 | 29 | 11 | 5.9 |  |
|  |  |  |  |  |  | 2.76 | 1.95 | 1.36 | 0.9 | 0.69 |  |
| 5 | 18000 |  |  |  |  |  | 83.4 | 35 | 13.3 | 7.1 | 2.2 |
|  |  |  |  |  |  |  | 2.17 | 1.51 | 1 | 0.77 | 0.47 |
| 5.5 | 19800 |  |  |  |  |  | 98.9 | 41.5 | 15.7 | 8.4 | 2.6 |
|  |  |  |  |  |  |  | 2.38 | 1.66 | 1.11 | 0.85 | 0.52 |
| 6 | 21600 |  |  |  |  |  | 115.6 | 48.4 | 18.4 | 9.8 | 3 |
|  |  |  |  |  |  |  | 2.6 | 1.81 | 1.21 | 0.93 | 0.57 |
| 6.5 | 23400 |  |  |  |  |  |  | 55.9 | 20.6 | 11.3 | 3.5 |
|  |  |  |  |  |  |  |  | 1.96 | 1.29 | 1 | 0.61 |
| 7 | 25200 |  |  |  |  |  |  | 63.8 | 24.2 | 12.9 | 4 |
|  |  |  |  |  |  |  |  | 2.11 | 1.41 | 1.08 | 0.66 |
| 7.5 | 27000 |  |  |  |  |  |  | 72.2 | 27.3 | 14.6 | 4.5 |
|  |  |  |  |  |  |  |  | 2.26 | 1.51 | 1.16 | 0.71 |
| 8 | 28800 |  |  |  |  |  |  | 81 | 30.7 | 16.3 | 5 |
|  |  |  |  |  |  |  |  | 2.41 | 1.61 | 1.24 | 0.75 |
| 9 | 32400 |  |  |  |  |  |  | 100 | 97.9 | 20.2 | 6.2 |
|  |  |  |  |  |  |  |  | 2.71 | 1.81 | 1.39 | 0.85 |
| 10 | 36000 |  |  |  |  |  |  |  | 45.8 | 24.4 | 7.5 |
|  |  |  |  |  |  |  |  |  | 2.01 | 1.54 | 0.94 |
| 11 | 39600 |  |  |  |  |  |  |  | 54.3 | 28.9 | 8.9 |
|  |  |  |  |  |  |  |  |  | 2.21 | 1.7 | 1.04 |
| 12 | 43200 |  |  |  |  |  |  |  | 63.5 | 33.8 | 10.4 |
|  |  |  |  |  |  |  |  |  | 2.41 | 1.85 | 1.13 |


| Flow rate |  | $\varphi$ - REPOLEN SDR 7.4 |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/s | kg/h | 25x3.5 | $32 \times 4.4$ | 40x5.5 | $50 \times 6.9$ | $63 \times 8.6$ | 75510.3 | 90x12.3 | 110x15.1 | 125517.1 | $160 \times 21.9$ |
| 13 | 46800 |  |  |  |  |  |  |  | 73.3 | 39 | 12 |
|  |  |  |  |  |  |  |  |  | 2.61 | 2.01 | 1.23 |
| 14 | 50400 |  |  |  |  |  |  |  |  | 44.5 | 13.6 |
|  |  |  |  |  |  |  |  |  |  | 2.16 | 1.32 |
| 15 | 54000 |  |  |  |  |  |  |  |  | 50.4 | 15.4 |
|  |  |  |  |  |  |  |  |  |  | 2.32 | 141 |
| 16 | 57600 |  |  |  |  |  |  |  |  | 56.6 | 17.1 |
|  |  |  |  |  |  |  |  |  |  | 2.47 | 1.5 |
| 17 | 61200 |  |  |  |  |  |  |  |  | 63.1 | 19.3 |
|  |  |  |  |  |  |  |  |  |  | 2.63 | 1.6 |
| 20 | 72000 |  |  |  |  |  |  |  |  |  | 25.9 |
|  |  |  |  |  |  |  |  |  |  |  | 1.89 |
| 30 | 108000 |  |  |  |  |  |  |  |  |  | 53.8 |
|  |  |  |  |  |  |  |  |  |  |  | 2.83 |

- REPOLEN SDR 9

The first value corresponds to the pressure drop in $\mathrm{mm} / \mathrm{m} . w . c$. and the second to the average speed in $\mathrm{m} / \mathrm{s}$.

| Flow rate |  | $\varphi$ - REPOLEN SDR 9 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/s | kg/h | 32x2.9 | 40x3.7 | 50x4.6 | $63 \times 5.8$ | 75x6. 8 | $90 \times 8.2$ |
| 0.1 | 360 | 3,78 | 1,33 |  |  |  |  |
|  |  | 0,21 | 0,13 |  |  |  |  |
| 0,15 | 540 | 7,49 | 2,63 |  |  |  |  |
|  |  | 0,31 | 0,2 |  |  |  |  |
| 0.2 | 720 | 12,22 | 4,28 | 1,49 | 0,51 |  |  |
|  |  | 0,41 | 0,26 | 0,17 | 0,11 |  |  |
| 0.3 | 1080 | 24,51 | 8,55 | 2,97 | 1,01 |  |  |
|  |  | 0,62 | 0,4 | 0,25 | 0,16 |  |  |
| 0.4 | 1440 | 40,33 | 14,03 | 4,86 | 1,65 |  |  |
|  |  | 0,83 | 0,53 | 0,34 | 0,21 |  |  |
| 0.5 | 1800 | 59,45 | 20,65 | 7,14 | 2,42 |  |  |
|  |  | 1,04 | 0,66 | 0,42 | 0,27 |  |  |
| 0,6 | 2160 | 81,74 | 28,35 | 9,79 | 3,31 |  |  |
|  |  | 1,24 | 0,79 | 0,51 | 0,32 |  |  |
| 0.7 | 2520 | 107,07 | 37,09 | 12,79 | 4,32 |  |  |
|  |  | 1,45 | 0,93 | 0,59 | 0,37 |  |  |
| 0.8 | 2880 | 135,36 | 46,85 | 16,14 | 5,44 |  |  |
|  |  | 1,66 | 1,06 | 0,68 | 0,43 |  |  |
| 0.9 | 3240 | 166,52 | 57,6 | 19,83 | 6,68 |  |  |
|  |  | 1,86 | 1,19 | 0,76 | 0,48 |  |  |
| 1 | 3600 | 200,51 | 69,3 | 23,84 | 8,03 |  |  |
|  |  | 2,07 | 1,32 | 0,85 | 0,53 |  |  |


| Flow rate |  | $\varphi$ - REPOLEN SDR 9 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/s | kgh | 32x.9 | $40 \times 3.7$ | 50x4.6 | $63 \times 5.8$ | 75x6. 8 | 90x8.2 |
| 1,1 | 3960 | 237,25 | 81,95 | 28,18 | 9,48 |  |  |
|  |  | 2,28 | 1,46 | 0,93 | 0,59 |  |  |
| 1.2 | 4320 | 276,7 | 95,53 | 32,82 | 11,04 |  |  |
|  |  | 2,48 | 1,59 | 1,01 | 0,64 |  |  |
| 1.3 | 4680 | 318,82 | 110,02 | 37,78 | 12,7 |  |  |
|  |  | 2,69 | 1,72 | 1,1 | 0,7 |  |  |
| 1.4 | 5040 | 363,57 | 125,4 | 43,05 | 14,46 |  |  |
|  |  | 2,9 | 1,85 | 1,18 | 0,75 |  |  |
| 1,5 | 5400 | 410,9 | 141,67 | 48,61 | 16,32 |  |  |
|  |  | 3,11 | 1,99 | 1,27 | 0,8 |  |  |
| 1.6 | 5760 | 460,8 | 158,82 | 54,47 | 18,28 |  |  |
|  |  | 3,31 | 2,12 | 1,35 | 0,86 |  |  |
| 1,7 | 6120 | 513,22 | 176,82 | 60,63 | 20,34 |  |  |
|  |  | 3,52 | 2,25 | 1,44 | 0,91 |  |  |
| 1.8 | 6480 | 568,14 | 195,68 | 67,07 | 22,49 |  |  |
|  |  | 3,73 | 2,38 | 1,52 | 0,96 |  |  |
| 1,9 | 6840 | 625,54 | 215,39 | 73,8 | 24,74 |  |  |
|  |  | 3,93 | 2,52 | 1,61 | 1,02 |  |  |
| 2 | 7200 | 685,38 | 235,93 | 80,81 | 27,08 | 11,71 |  |
|  |  | 4,14 | 2,65 | 1,69 | 1,07 | 0,75 |  |
| 2.2 | 7920 |  | 279,49 | 95,68 | 32,05 | 13,84 |  |
|  |  |  | 2,91 | 1,86 | 1,18 | 0,83 |  |
| 2.4 | 8640 |  | 326,3 | 111,66 | 37,38 | 16,14 |  |
|  |  |  | 3,18 | 2,03 | 1,28 | 0,9 |  |
| 2.6 | 9360 |  | 376,33 | 128,72 | 43,07 | 18,59 |  |
|  |  |  | 3,44 | 2,2 | 1,39 | 0,98 |  |
| 2.8 | 10080 |  | 429,51 | 146,85 | 49,11 | 21,19 |  |
|  |  |  | 3,71 | 2,37 | 1,5 | 1,05 |  |
| 3 | 10800 |  | 485,81 | 166,04 | 55,51 | 23,95 | 10,07 |
|  |  |  | 3,97 | 2,54 | 1,6 | 1,13 | 0,78 |
| 3.5 | 12600 |  |  | 218,56 | 73 | 31,47 | 13,22 |
|  |  |  |  | 2,96 | 1,87 | 1,32 | 0,91 |
| 4 | 14400 |  |  | 277,42 | 92,6 | 39,89 | 16,75 |
|  |  |  |  | 3,38 | 2,14 | 1,5 | 1,05 |
| 4.5 | 16200 |  |  | 342,49 | 114,25 | 49,2 | 20,64 |
|  |  |  |  | 3,81 | 2,41 | 1,69 | 1,18 |
| 5 | 18000 |  |  |  | 137,91 | 59,36 | 24,89 |
|  |  |  |  |  | 2,67 | 1,88 | 1,31 |
| 6 | 21600 |  |  |  | 191,11 | 82,2 | 34,45 |
|  |  |  |  |  | 3,21 | 2,26 | 1,57 |
| 7 | 25200 |  |  |  | 251,96 | 108,31 | 45,36 |
|  |  |  |  |  | 3,74 | 2,63 | 1,83 |
| 8 | 28800 |  |  |  |  | 137,6 | 57,59 |
|  |  |  |  |  |  | 3,01 | 2,09 |


| Flow rate |  | $\varphi$ - REPOLEN SDR 9 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/s | kg/4 | 32x. 29 | 40x3.7 | 50x4.6 | $63 \times 5.8$ | $75 \times 6.8$ | $90 \times 8.2$ |
| 9 | 32400 |  |  |  |  | 169,99 | 71,12 |
|  |  |  |  |  |  | 3,38 | 2,35 |
| 10 | 36000 |  |  |  |  | 205,44 | 85,92 |
|  |  |  |  |  |  | 3,76 | 2,6 |
| 11 | 39600 |  |  |  |  |  | 101,95 |
|  |  |  |  |  |  |  | 2,87 |
| 12 | 43200 |  |  |  |  |  | 119,22 |
|  |  |  |  |  |  |  | 3,14 |
| 13 | 46800 |  |  |  |  |  | 137,68 |
|  |  |  |  |  |  |  | 3,4 |
| 14 | 50400 |  |  |  |  |  | 157,34 |
|  |  |  |  |  |  |  | 3,66 |

■ REPOLEN SDR 11
The first value corresponds to the pressure drop in $\mathrm{mm} / \mathrm{m} . \mathrm{w}$. . . and the second to the average speed in $\mathrm{m} / \mathrm{s}$.

| Flow rate |  | $\varphi$ - REPOLEN SDR 11 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I/s | kgh | 32x2.9 | 40x3.7 | 50x4.6 | 63x5.8 | $75 \times 6.8$ | 90x8.2 | 110x10 | 125x11.4 | $160 \times 14.6$ |
| 0.1 | 360 | 2.9 |  |  |  |  |  |  |  |  |
|  |  | 0.19 |  |  |  |  |  |  |  |  |
| 0.16 | 576 | 6.5 |  |  |  |  |  |  |  |  |
|  |  | 0.3 |  |  |  |  |  |  |  |  |
| 0.2 | 720 | 9.4 |  |  |  |  |  |  |  |  |
|  |  | 0.37 |  |  |  |  |  |  |  |  |
| 0.25 | 864 | 13.8 |  |  |  |  |  |  |  |  |
|  |  | 0.46 |  |  |  |  |  |  |  |  |
| 0.3 | 1080 | 18.9 | 6.7 |  |  |  |  |  |  |  |
|  |  | 0.56 | 0.36 |  |  |  |  |  |  |  |
| 0.35 | 1260 | 24.7 | 8.8 |  |  |  |  |  |  |  |
|  |  | 0.65 | 0.42 |  |  |  |  |  |  |  |
| 0.4 | 1440 | 31.1 | 11.1 | 3.8 |  |  |  |  |  |  |
|  |  | 0.74 | 0.48 | 0.31 |  |  |  |  |  |  |
| 0.45 | 1620 | 38.1 | 13.6 | 4.7 |  |  |  |  |  |  |
|  |  | 0.83 | 0.6 | 0.34 |  |  |  |  |  |  |
| 0.5 | 1800 | 45.8 | 16.3 | 5.6 |  |  |  |  |  |  |
|  |  | 0.93 | 0.6 | 0.38 |  |  |  |  |  |  |
| 0.55 | 1980 | 54.1 | 19.2 | 6.6 |  |  |  |  |  |  |
|  |  | 1.02 | 0.66 | 0.42 |  |  |  |  |  |  |
| 0.6 | 2160 | 63 | 22.3 | 7.7 |  |  |  |  |  |  |
|  |  | 1.11 | 0.72 | 0.46 |  |  |  |  |  |  |


| Flow rate |  | $\varphi$ - REPOLEN SDR 11 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/s | kg/h | $32 \times 2.9$ | 40x3.7 | 50x46 | ${ }_{63 \times 5.8}$ | 75x6.8 | 9008.2 | 110x10 | 125511.4 | $160 \times 14.6$ |
| 0.65 | 2340 | 72.1 | 25.7 | 8.9 | 3 |  |  |  |  |  |
|  |  | 1.21 | 0.78 | 0.5 | 0.31 |  |  |  |  |  |
| 0.7 | 2520 | 82.5 | 29.2 | 10.1 | 3.4 |  |  |  |  |  |
|  |  | 1.3 | 0.84 | 0.54 | 0.34 |  |  |  |  |  |
| 0.75 | 2700 | 93.1 | 33 | 11.4 | 3.8 |  |  |  |  |  |
|  |  | 1.39 | 0.9 | 0.57 | 0.36 |  |  |  |  |  |
| 0.8 | 2880 | 104.2 | 36.9 | 12.7 | 4.3 |  |  |  |  |  |
|  |  | 1.48 | 0.96 | 0.61 | 0.39 |  |  |  |  |  |
| 0.85 | 3060 | 116 | 41 | 14.1 | 4.7 |  |  |  |  |  |
|  |  | 1.58 | 1.02 | 0.65 | 0.41 |  |  |  |  |  |
| 0.9 | 3240 |  | 45.3 | 15.6 | 5.2 |  |  |  |  |  |
|  |  |  | 1.08 | 0.69 | 0.43 |  |  |  |  |  |
| 1 | 3600 |  | 54.5 | 18.8 | 6.3 | 2.7 |  |  |  |  |
|  |  |  | 1.2 | 0.76 | 0.48 | 0.34 |  |  |  |  |
| 1.2 | 4320 |  | 75.2 | 25.8 | 8.6 | 3.7 |  |  |  |  |
|  |  |  | 1.44 | 0.92 | 0.58 | 0.41 |  |  |  |  |
| 1.4 | 5040 |  | 98.7 | 33.9 | 11.3 | 4.9 | 2.1 |  |  |  |
|  |  |  | 1.68 | 1.07 | 0.67 | 0.47 | 0.33 |  |  |  |
| 1.6 | 5760 |  |  | 42.9 | 14.3 | 6.1 | 2.6 |  |  |  |
|  |  |  |  | 1.22 | 0.77 | 0.54 | 0.38 |  |  |  |
| 1.8 | 6480 |  |  | 52.8 | 21.1 | 9.1 | 3.8 |  |  |  |
|  |  |  |  | 1.38 | 0.96 | 0.68 | 0.47 |  |  |  |
| 2 | 7200 |  |  | 63.6 | 25 | 9.1 | 3.8 |  |  |  |
|  |  |  |  | 1.53 | 1.06 | 0.68 | 0.47 |  |  |  |
| 2.2 | 7920 |  |  | 73.2 | 25 | 10.7 | 4.5 |  |  |  |
|  |  |  |  | 1.68 | 1.06 | 0.74 | 0.52 |  |  |  |
| 2.4 | 8640 |  |  |  | 29.2 | 12.5 | 5.3 |  |  |  |
|  |  |  |  |  | 1.16 | 0.81 | 0.56 |  |  |  |
| 2.6 | 9360 |  |  |  | 33.6 | 14.4 | 6.0 |  |  |  |
|  |  |  |  |  | 1.25 | 0.9 | 0.6 |  |  |  |
| 2.8 | 10080 |  |  |  | 38.3 | 16.4 | 6.9 | 2.7 |  |  |
|  |  |  |  |  | 1.35 | 0.9 | 0.7 | 0.4 |  |  |
| 3 | 10800 |  |  |  | 43.3 | 18.5 | 7.8 | 3 | 1.6 |  |
|  |  |  |  |  | 1.45 | 1.01 | 0.71 | 0.47 | 0.37 |  |
| 3.5 | 12600 |  |  |  | 57 | 24.4 | 10.3 | 3.9 | 2.1 |  |
|  |  |  |  |  | 1.69 | 1.18 | 0.9 | 0.55 | 0.43 |  |
| 4 | 14400 |  |  |  | 72.2 | 30.9 | 13 | 5 | 2.7 |  |
|  |  |  |  |  | 1.93 | 1.4 | 0.9 | 0.6 | 0.5 |  |
| 4.5 | 16200 |  |  |  |  | 38.1 | 16 | 6.1 | 3.3 |  |
|  |  |  |  |  |  | 1.5 | 1.1 | 0.7 | 0.5 |  |
| 5 | 18000 |  |  |  |  | 46 | 19.3 | 7.4 | 4 | 1.2 |
|  |  |  |  |  |  | 1.69 | 1.18 | 0.79 | 0.61 | 0.37 |
| 5.5 | 19800 |  |  |  |  | 54.5 | 22.9 | 8.8 | 4.8 | 1.5 |
|  |  |  |  |  |  | 1.86 | 1.29 | 0.86 | 0.67 | 0.41 |



The pressure drop stipulated for the fittings is:

| Description | Scheme | Resistance coefficient ( r ) |
| :---: | :---: | :---: |
| Sleeve |  | 0.25 |
| Sleeve Thread - Female | $\square$ | 0.5 |
| Sleeve Thread - Male |  | 0.7 |
| One diameter reducer |  | 0.4 |
| Two diameter reducer |  | 0.5 |
| Three diameter reducer |  | 0.6 |
| Four diameter reducer | - | 0.7 |
| Five diameter reducer |  | 0.8 |
| Six diameter reducer |  | 0.9 |
| $90^{\circ}$ Elbow |  | 1.2 |
| $90^{\circ}$ Elbow Thread - Male | ${ }_{4}^{\omega}$ | 1.6 |
| $90^{\circ}$ Elbow Thread - Female | ${ }^{\mathrm{m}}$ | 1.4 |
| $45^{\circ}$ Elbow | $1$ | 0.6 |
| Divergent Flow Tee | $\underset{\rightarrow}{\rightarrow}$ | 1.8 |
| Convergent Flow Tee | $\underset{\rightarrow}{\rightarrow}$ | 1.3 |
| Opposition Tee with Divergent Flow | $\underset{\leftarrow}{\stackrel{+}{4}}$ | 2.2 |
| Opposition Tee with Convergent Flow | $\underset{\rightarrow}{\rightarrow}+$ | 4.2 |
| Reducing tee | The resul | with the reducer |
| Female thread tee | $\underset{\rightarrow}{\neq 1}$ | 1.6 |
| Tee Thread - Male | $\underset{\rightarrow}{\exists} \underset{\square}{\xi}$ | 1.8 |

## - Example

Assume an installation with 10 linear meters of REPOLEN pipe and a $25 \times 4.2 \mathrm{~mm}$ diameter, in which there are 4 sleeves, $390^{\circ}$ elbows, 2 tees and a female threaded sleeve, which is intended to transport $0.351 /$ s of water at $10^{\circ} \mathrm{C}$

The total pressure drop will be the pressure drop of the piping, plus that of the fittings:

```
H=Ht+Ha
```

where: $\quad H$ is the total pressure drop in mm.w.c.
Ht is the pressure drop of the piping in mm.w.c.
Ha is the pressure drop of the fittings in mm.w.c.
For calculating the pressure drop of the piping it is necessary to consult the previous tables, so we see that for the chosen pipe and $0.35 / /$ s, we have a water velocity of $1.65 \mathrm{~m} / \mathrm{s}$ and a pressure drop of 149 mm .w.c. Since we have 10 linear meters:

## $\mathrm{Ht}=149 * 10=1490$ mm.w.c.

The pressure drop of various fittings is calculated by the equation

$$
\mathrm{Ha}=\Sigma \mathrm{r} * \mathrm{v}^{2} * \gamma^{\prime}{ }_{2 * \mathrm{~g}}
$$

where: $r$ is the coefficient of resistance of the fitting
v is the velocity of the transported fluid in $\mathrm{m} / \mathrm{s}$
Y is the specific weight of the fluid transported. Being water is $1 \mathrm{~kg} / \mathrm{l}$ g is the acceleration of gravity, $9.8 \mathrm{~m} / \mathrm{s}$
$\mathrm{Ha}=(4 * 0.25+3 * 1.2 * 2 * 1.8+0.5) * 1.65^{2} * \frac{1}{2} 2 * 9.8=8.7 * 2.72 * 0.05=1.183$ m.c.a. $=1183 \mathrm{~mm}$. w.c.
$H=1490+1183=2673 \mathrm{~mm}$. w.c.

### 7.7 PEAK FLOW RATE

Determination of peak flow rate Vs from the sum of flows VVR for residential buildings
acc. to DIN 1988 Teil 3 VS $=0.682-(\Sigma V R) 0.45-0.7[1 / \mathrm{s}]$

| 2VR | vs | EVR | vs | EVR | vs | EVR | vs | EVR | vs | 2VR | vs | 2VR | vs | EVR | vs |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0,03 | 0,00 | 1,02 | 0,55 | 2,02 | 0,80 | 3,02 | 0,98 | 4,02 | 1,14 | 5,10 | 1,28 | 10,10 | 1,79 | 15,10 | , 17 |
| 0,04 | 0,02 | 1,04 | 0,55 | 2,04 | 0,80 | 3,04 | 0,98 | 4,04 | 1,14 | 5,20 | 1,29 | 10,20 | 1,80 | 15,20 | 2,18 |
| 0,06 | 0,05 | 1,06 | 0,56 | 2,06 | 0,80 | 3,06 | 0,99 | 4,06 | 1,14 | 5,30 | 1,30 | 10,30 | 1,81 | 15,30 | 2,19 |
| 0,07 | 0,07 | 1,08 | 0,57 | 2,08 | 0,81 | 3,08 | 0,99 | 4,08 | 1,14 | 5,40 | 1,32 | 10,40 | 1,82 | 15,40 | 2,19 |
| 0,08 | 0,08 | 1,10 | 0,57 | 2,10 | 0,81 | 3,10 | 0,99 | 4,10 | 1,15 | 5,50 | 1,33 | 10,50 | 1,82 | 15,50 | 2,20 |
| 0,09 | 0,09 | 1,12 | 0,58 | 2,12 | 0,82 | 3,12 | 1,00 | 4,12 | 1,15 | 5,60 | 1,34 | 10,60 | 1,83 | 15,60 | 2,21 |
| 0,10 | 0,10 | 1,14 | 0,58 | 2,14 | 0,82 | 3,14 | 1,00 | 4,14 | 1,15 | 5,70 | 1,35 | 10,70 | 1,84 | 15,70 | 2,21 |
| 0,13 | 0,13 | 1,16 | 0,59 | 2,16 | 0,82 | 3,16 | 1,00 | 4,16 | 1,16 | 5,80 | 1,36 | 10,80 | 1,85 | 15,80 | 2,22 |
| 0,15 | 0,15 | 1,18 | 0,59 | 2,18 | 0,83 | 3,18 | 1,01 | 4,18 | 1,16 | 5,90 | 1,38 | 10,90 | 1,86 | 15,90 | 2,23 |
| 0,20 | 0,19 | 1,20 | 0,60 | 2,20 | 0,83 | 3,20 | 1,01 | 4,20 | 1,16 | 6,00 | 1,39 | 11,00 | 1,87 | 16,00 | 2,23 |
| 0,22 | 0,21 | 1,22 | 0,61 | 2,22 | 0,84 | 3,22 | 1,01 | 4,22 | 1,16 | 6,10 | 1,40 | 11,10 | 1,87 | 16,10 | 2,24 |
| 0,24 | 0,22 | 1,24 | 0,61 | 2,24 | 0,84 | 3,24 | 1,02 | 4,24 | 1,17 | 6,20 | 1,41 | 11,20 | 1,88 | 16,20 | 2,25 |
| 0,26 | 0,23 | 1,26 | 0,62 | 2,26 | 0,84 | 3,26 | 1,02 | 4,26 | 1,17 | 6,30 | 1,42 | 11,30 | 1,89 | 16,30 | 2,25 |
| 0,28 | 0,24 | 1,28 | 0,62 | 2,28 | 0,85 | 3,28 | 1,02 | 4,28 | 1,17 | 6,40 | 1,43 | 11,40 | 1,90 | 16,40 | 2,26 |
| 0,30 | 0,26 | 1,30 | 0,63 | 2,30 | 0,85 | 3,30 | 1,03 | 4,30 | 1,17 | 6,50 | 1,44 | 11,50 | 1,91 | 16,50 | 2,27 |
| 0,32 | 0,27 | 1,32 | 0,63 | 2,32 | 0,86 | 3,32 | 1,03 | 4,32 | 1,18 | 6,60 | 1,45 | 11,60 | 1,91 | 16,60 | 2,27 |
| 0,34 | 0,28 | 1,34 | 0,64 | 2,34 | 0,86 | 3,34 | 1,03 | 4,34 | 1,18 | 6,70 | 1,47 | 11,70 | 1,92 | 16,70 | 2,28 |
| 0,36 | 0,29 | 1,36 | 0,64 | 2,36 | 0,86 | 3,36 | 1,04 | 4,36 | 1,18 | 6,80 | 1,48 | 11,80 | 1,93 | 16,80 | 2,29 |
| 0,38 | 0,30 | 1,38 | 0,65 | 2,38 | 0,87 | 3,38 | 1,04 | 4,38 | 1,19 | 6,90 | 1,49 | 11,90 | 1,94 | 16,90 | 2,29 |
| 0,40 | 0,31 | 1,40 | 0,65 | 2,40 | 0,87 | 3,40 | 1,04 | 4,40 | 1,19 | 7,00 | 1,50 | 12,00 | 1,95 | 17,00 | 2,30 |
| 0,42 | 0,32 | 1,42 | 0,66 | 2,42 | 0,88 | 3,42 | 1,05 | 4,42 | 1,19 | 7,10 | 1,51 | 12,10 | 1,95 | 17,10 | 2,31 |
| 0,44 | 0,33 | 1,44 | 0,66 | 2,44 | 0,88 | 3,44 | 1,05 | 4,44 | 1,19 | 7,20 | 1,52 | 12,20 | 1,96 | 17,20 | 2,31 |
| 0,46 | 0,34 | 1,46 | 0,67 | 2,46 | 0,88 | 3,46 | 1,05 | 4,46 | 1,20 | 7,30 | 1,53 | 12,30 | 1,97 | 17,30 | 2,32 |
| 0,48 | 0,35 | 1,48 | 0,67 | 2,48 | 0,89 | 3,48 | 1,06 | 4,48 | 1,20 | 7,40 | 1,54 | 12,40 | 1,98 | 17,40 | 2,33 |
| 0,50 | 0,36 | 1,50 | 0,68 | 2,50 | 0,89 | 3,50 | 1,06 | 4,50 | 1,20 | 7,50 | 1,55 | 12,50 | 1,99 | 17,50 | 2,33 |
| 0,52 | 0,37 | 1,52 | 0,68 | 2,52 | 0,89 | 3,52 | 1,06 | 4,52 | 1,20 | 7,60 | 1,56 | 12,60 | 1,99 | 17,60 | 2,34 |
| 0,54 | 0,38 | 1,54 | 0,69 | 2,54 | 0,90 | 3,54 | 1,06 | 4,54 | 1,21 | 7,70 | 1,57 | 12,70 | 2,00 | 17,70 | 2,35 |
| 0,56 | 0,39 | 1,56 | 0,69 | 2,56 | 0,90 | 3,56 | 1,07 | 4,56 | 1,21 | 7,80 | 1,58 | 12,80 | 2,01 | 17,80 | 2,35 |
| 0,58 | 0,39 | 1,58 | 0,70 | 2,58 | 0,90 | 3,58 | 1,07 | 4,58 | 1,21 | 7,90 | 1,59 | 12,90 | 2,02 | 17,90 | 2,36 |
| 0,60 | 0,40 | 1,60 | 0,70 | 2,60 | 0,91 | 3,60 | 1,07 | 4,60 | 1,22 | 8,00 | 1,60 | 13,00 | 2,02 | 18,00 | 2,36 |
| 0,62 | 0,41 | 1,62 | 0,71 | 2,62 | 0,91 | 3,62 | 1,08 | 4,62 | 1,22 | 8,10 | 1,61 | 13,10 | 2,03 | 18,10 | 2,37 |
| 0,64 | 0,42 | 1,64 | 0,71 | 2,64 | 0,92 | 3,64 | 1,08 | 4,64 | 1,22 | 8,20 | 1,62 | 13,20 | 2,04 | 18,20 | 2,38 |
| 0,66 | 0,43 | 1,66 | 0,72 | 2,66 | 0,92 | 3,66 | 1,08 | 4,66 | 1,22 | 8,30 | 1,63 | 13,30 | 2,05 | 18,30 | 2,38 |
| 0,68 | 0,43 | 1,68 | 0,72 | 2,68 | 0,92 | 3,68 | 1,09 | 4,68 | 1,23 | 8,40 | 1,64 | 13,40 | 2,05 | 18,40 | 2,39 |
| 0,70 | 0,44 | 1,70 | 0,73 | 2,70 | 0,93 | 3,70 | 1,09 | 4,70 | 1,23 | 8,50 | 1,65 | 13,50 | 2,06 | 18,50 | 2,40 |
| 0,72 | 0,45 | 1,72 | 0,73 | 2,72 | 0,93 | 3,72 | 1,09 | 4,72 | 1,23 | 8,60 | 1,66 | 13,60 | 2,07 | 18,60 | 2,40 |
| 0,74 | 0,46 | 1,74 | 0,74 | 2,74 | 0,93 | 3,74 | 1,09 | 4,74 | 1,23 | 8,70 | 1,67 | 13,70 | 2,07 | 18,70 | 2,41 |
| 0,76 | 0,46 | 1,76 | 0,74 | 2,76 | 0,94 | 3,76 | 1,10 | 4,76 | 1,24 | 8,80 | 1,67 | 13,80 | 2,08 | 18,80 | 2,41 |
| 0,78 | 0,47 | 1,78 | 0,74 | 2,78 | 0,94 | 3,78 | 1,10 | 4,78 | 1,24 | 8,90 | 1,68 | 13,90 | 2,09 | 18,90 | 2,42 |
| 0,80 | 0,48 | 1,80 | 0,75 | 2,80 | 0,94 | 3,80 | 1,10 | 4,80 | 1,24 | 9,00 | 1,69 | 14,00 | 2,10 | 19,00 | 2,43 |
| 0,82 | 0,48 | 1,82 | 0,75 | 2,82 | 0,95 | 3,82 | 1,11 | 4,82 | 1,24 | 9,10 | 1,70 | 14,10 | 2,10 | 19,10 | 2,43 |
| 0,84 | 0,49 | 1,84 | 0,76 | 2,84 | 0,95 | 3,84 | 1,11 | 4,84 | 1,25 | 9,20 | 1,71 | 14,20 | 2,11 | 19,20 | 2,44 |
| 0,86 | 0,50 | 1,86 | 0,76 | 2,86 | 0,95 | 3,86 | 1,11 | 4,86 | 1,25 | 9,30 | 1,72 | 14,30 | 2,21 | 19,30 | 2,44 |
| 0,88 | 0,50 | 1,88 | 0,77 | 2,88 | 0,96 | 3,88 | 1,12 | 4,88 | 1,25 | 9,40 | 1,73 | 14,40 | 2,12 | 19,40 | 2,45 |
| 0,90 | 0,51 | 1,90 | 0,77 | 2,90 | 0,96 | 3,90 | 1,12 | 4,90 | 1,25 | 9,50 | 1,74 | 14,50 | 2,13 | 19,50 | 2,46 |
| 0,92 | 0,52 | 1,92 | 0,77 | 2,92 | 0,96 | 3,92 | 1,12 | 4,92 | 1,26 | 9,60 | 1,75 | 14,60 | 2,14 | 19,60 | 2,46 |
| 0,94 | 0,52 | 1,94 | 0,78 | 2,94 | 0,97 | 3,94 | 1,12 | 4,94 | 1,26 | 9,70 | 1,76 | 14,70 | 2,15 | 19,70 | 2,47 |
| 0,96 | 0,53 | 1,96 | 0,78 | 2,96 | 0,97 | 3,96 | 1,13 | 4,96 | 1,26 | 9,80 | 1,76 | 14,80 | 2,15 | 19,80 | 2,47 |
| 0,98 | 0,54 | 1,98 | 0,79 | 2,98 | 0,97 | 3,98 | 1,13 | 4,98 | 1,26 | 9,90 | 1,77 | 14,90 | 2,16 | 19,90 | 2,48 |
| 1,00 | 0,54 | 2,00 | 0,79 | 3,00 | 0,98 | 4,00 | 1,13 | 5,00 | 1,27 | 10,00 | 1,78 | 15,00 | 2,17 | 20,00 | 2,49 |

*This table is valid when the flow rate VR of the individual intake points is less than $0.51 / \mathrm{s}$.

Determination of peak flow rate Vs from the sum of flows SVR for residential buildings
acc. to DIN 1988 Teil 3 VS $=1.7-(\Sigma V R) 0.21-0.7[1 / \mathrm{s}]$

* This table is valid when the flow rate VR of the individual intake points is less than $0.51 / \mathrm{s}$.


### 7.8 INSTALLATIONS SIIING

According to CTE HS4, the flow rates to be taken into consideration are:

| Equipment | Minimum instantaneous flow rate (1/s) |  | Nominal diameter of the coupling submain |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Cold water | Hot water (Hot Water System) | Steel pipe (") | Copper or plastic pipe (mm) |
| Bathtub < 1.4 m | 0.2 | 0.15 | 3/4 | 20 |
| Bathtub>1.4 m | 0.3 | 0.2 | 3/4 | 20 |
| Bidet | 0.1 | 0.065 | 1/2 | 12 |
| Shower | 0.2 | 0.1 | 1/2 | 12 |
| Domestic sink | 0.2 | 0.1 | 1/2 | 12 |
| Non-domestic sink | 0.3 | 0.2 | 3/4 | 20 |
| Isolated tap | 0.15 | 0.1 | --- | --- |
| Garage tap | 0.2 | --- | --- | --- |
| Toilet with cistern | 0.1 | --- | 1/2 | 12 |
| Toilet with flushometer | 1.25 | --- | 1-1/2 | 25-40 |
| Toilet | 0.1 | 0.065 | 1/2 | 12 |
| Laundry foom | 0.2 | 0.1 | --- | --- |
| Domestic washing machine | 0.2 | 0.15 | 3/4 | 20 |
| Industrial washing machine ( $>8 \mathrm{~kg}$ ) | 0.6 | 0.4 | 1 | 25 |
| Washbasin | 0.05 | 0.03 | 1/2 | 12 |
| Domestic dishwasher | 0.15 | 0.1 | $1 / 2\left(\right.$ thread to ${ }^{3 / 4}$ ) | 12 |
| Industrial dishwasher (20 services) | 0.25 | 0.2 | 3/4 | 20 |
| Urinal with cistern | 0.04 | --- | 1/2 | 12 |
| Urinal with timed tap | 0.15 | --- | 1/2 | 12 |
| Landfill | 0.2 | --- | 3/4 | 20 |

$\square$ The minimum pressures will be:
100 kPa for common taps
150 kPa for flushometers and heaters
The pressure at any point of consumption must not exceed 500 kPa .

The temperature at the Hot Water System points of consumption must be between 50 and $65^{\circ} \mathrm{C}$.
$\square$ The installations will be sized by dividing the installation into sections and always taking into account the most unfavourable section (the one with the greatest pressure loss).
The calculation speed must be between 0.5 and $3.5 \mathrm{~m} / \mathrm{s}$ (for plastic piping).
$\square$ The minimum supply diameters are

For the Hot Water System, the drive circuit is calculated in the same way as for cold water. For the return circuit, the flow rate will be estimated so that in the most distant tap, the temperature loss is a maximum of $3^{\circ} \mathrm{C}$ from the outlet of the accumulator or exchanger.

In any case, no less than $2501 / \mathrm{h}$ will be recirculated in each column. It must be considered that at least $10 \%$ of the supply water is recirculated. The minimum internal diameter of the return piping must be 16 mm .

The diameters on the recirculated flow rate are:

| Piping diameter (") | Recirculated flow rate (l/h) |
| :---: | :---: |
| $1 / 2$ | 14 |
| $3 / 4$ | 300 |
| 1 | 600 |
| $11 / 4$ | 1100 |
| $1 / 2$ | 1800 |
| 2 | 3300 |

## ON-SITE RECOMMENDATIONS 7.9

Take into account the environmental conditions when welding, avoiding currents that could cause undesirable cooling
$\square$ PPR REPOLEN pipes must never be exposed to direct sunlight, as they are not protected against ultraviolet radiation.

- In case of low temperatures, check the condition of the pipes' ends, in case any unintended impact could have occurred during handing or transport.
- PPR REPOLEN pipes can be installed in direct contact with any traditional building material.

Take special care with regard to lineal expansions, both in recessed installations and in exposed installations, to allow for movement and to place the fasteners where necessary and advisable.
In the case of buried installations, they must be placed at a 0.8 m depth if traffic will not run over them and at 1 m if it may run over them.


## CONNECTION SYSTEMS

8.1 Thermofusion or socket welding connection
8.2 Butt weld connection
. 3 Electrofusion connectio
8.4 Flanged systems
8.5 Installation of branch systems
8.6 System repair

The main connection system are:
Thermofusion or socket welding (recommended option)

## Electrofusion

Butt or mirror welding
Others: flanged fittings, threads, etc.

For most of these systems, there are a series of common points to keep in mind:

It is essential to maintain the cleanliness of the elements to be connected. Such cleaning should never be done using chemicals. Wiping off any dirt with a clean cloth would be enough. The cuts of the parts to be joined must be as parallel as possible to each other and as perpendicular as possible to the length of the pipe. If there is any burr, it is advisable to remove it before connecting the parts.
In processes where temperature is involved, it is important to ensure that materials with similar melting points are to be connected.
is necessary to consider the en place, since extreme temperatures could distort machine data in automatic welds, or even affect the elements to be joined. In the same way, it is necessary to avoid air currents that can make the connection difficult, since it may accelerate the partial cooling of the different elements.

### 8.1 THERMOFUSION OR SOCKET WELDING

The process consists of connecting a pipe and a fitting by applying heat on the external part of the pipe and the internal part of the fitting. To do this, the pipe is inserted into the heating matrix while another heating matrix is inserted into the fitting.

Once the corresponding time has elapsed (see time table), the matrices are removed and the pipe is inserted into the fitting, keeping the pressure for the indicated time

This type of welding guarantees a perfect pipe - fitting connection. The end result is a single part, eliminating the risk of leakage.
maintaining the pressure for the time indicated in the table. During this time, small alignment corrections can be made. When the bench welder is used (large diameters), the procedure is almost the same, except that the pressure is exerted by the bench. A good weld will produce a uniform bead all around the welded perimeter (see butt weld bead) Wait about two hours before doing hydraulic tests.
and allowing the material to melt slowly
Count the time indicated in the enclosed table according to the diameter of the pipe

Remove the pipe and fitting and insert the pipe into the fitting,
Check the temperature of the matrices $\left(275-285^{\circ} \mathrm{C}\right)$. It is necessary to avoid air currents that could cool the matrix on one side. The temperature difference does not guarantee a good weld.
Clean the pipe and fitting with a clean cloth
Mark the depth at which the pipe should enter
Mark the depth at which the pipe should enter
Insert the pipe and fitting while exerting a light pressure on them

$\square$ Steps for machine welding




Insert the pipe into the fitting



Note: It is recommended to wait at leasta couple of hours before testing for leaks.

special care of the heating matrices

- It is important to keep them in good condition, preventing them from suffering any impact or scratches.
- Always keep them clean. If there is any material attached left, remove it while they are still hot using a clean cloth.
- If they are used for more than one material, cleaning when finished is especially important.

The procedure consists of heating two pipes (or a pipe with a fitting of the same outer diameter and thickness as the pipe) by means of a heating plate, and then apply pressure to achieve the connection of both elements.
It is usually used for large diameters. It is very important that it is always carried out between equal thicknesses and diameters.

## $\square$ Welding instructions

- Place the elements aligned on the welding machine.
- Face the pipes (using the blade of the machine itself) to properly clean the surfaces and even them out.
- Remove the facing tool and the burrs without touching the surfaces to be connected.
Ensure the surfaces are parallel to each other.
- Check that the heating plate is clean and at the correct temperature.
- Follow the pressure curve indicated by the machine manufacturer.
- A first P1 pressure is exerted for a T1 time to create the initial height cord (h).
- After this time, lower the pressure to ensure full heating P2 (preset
welding pressure $=1.5$ bar)
After the heating time T , move back the elements and remove the heating plate and quickly connect the ends T3.
- Increase the pressure progressively until it reaches the pressure indicated by the manufacturer P1 - T4
Maintain this pressure for the time indicated until the weld is cold T5.
Wait about two hours before doing hydraulic test.


The system consists of passing a low voltage current throug metal coils inside the fittings, embedded in the polypropylene, causing the Joule heating effect that welds the fitting with the pipe previously inserted in it.
 inserted without forcing it but play-free).


Reboca, S.L. has flanged systems that enable the connection between pipes. REPOLEN flanges are PN16.
Remember that the tightening of the screws must always be done crosswise and gradually, in order to ensure a perfect coupling of the gasket.

| Measure | PN | Thickness $(\mathrm{mm})$ | Outer diameter $(\mathrm{mm})$ | Internal diameter $(\mathrm{mm})$ | No. of holes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 32 | 16 | 16,8 | 117 | 42,5 | 4 |
| 40 | 16 | 18 | 141,5 | 51 | 4 |
| 50 | 16 | 18 | 151 | 62,5 | 4 |
| 63 | 16 | 19,5 | 165 | 78 | 4 |
| 75 | 16 | 19,5 | 188,5 | 93 | 4 |
| 90 | 16 | 19,5 | 199 | 113 | 8 |
| 110 | 16 | 19,5 | 224,5 | 134 | 8 |
| 125 | 16 | 25 | 250 | 168 | 8 |
| 140 | 16 | 25 | 250 | 159 | 8 |
| 160 PPR | 16 | 19,5 | 285 | 191,5 | 8 |
| 160 PE | 16 | 19,5 | 285 | 179,5 | 8 |
| 200 | 16 | 24 | 341,5 | 236 | 12 |
| 250 | 16 | 30 | 404,5 | 288,5 | 12 |
| 315 | 16 | 34 | 462,5 | 338 | 12 |



### 8.5 INSTALLATION OF BRANCH SYSTEMS

Make a hole in the pipe where you want to make the new intake with the corresponding drill.


Apply the heating matrices both to the pipe and to the branch to be grafted, proceeding in the same way as with any socket weld.


Cut the edges that may remain carefully so as not to damage the pipe.


Remove the matrices and insert the branch into the hole.



Cut off excess plug.


The hole has to be round.


Insert the plug into the hole taking care not to insert it too much so as not to create turbulence in the water flow.


Finished look.


ANNEXES

### 9.1 CHEMICAL RESISTANCE TABLE

| + | Resists with insignificant variations |  |  |
| :--- | :--- | :--- | :--- |
| cold sat. | Cold saturation |  |  |
| ( Resists with variations under certain conditions | e | Boiling |  |
| - | Does not resist | a | Aqueous solution |


| product | concent | temprature |  |  | product | CONCENT. | темperature |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | \% | $20^{\circ} \mathrm{C}$ | anc | ${ }^{1000}$ |  |  | 20 C | 600 | 1ome |
| Oil No. 3 according to ASMT D380-59 | 100 | + | 1 | - | Acetic Acid | 70 | + | + |  |
| Camphor oil |  |  |  |  |  | 50 | + | + |  |
| Animal oil |  | + | + |  |  | 30 | + | + |  |
| Peanut oil | 100 | + | + | 1 |  | 10 | + | + | + |
| Coconut oil |  | + | + |  | Battery acid | $\mathrm{d}=1,28$ | + | + |  |
| Fish liver oil |  | + |  |  | Adipic acid | a. | + | + |  |
| Flaxsed oil | 100 | + | + | + | Anthraquinon-sulfonic acid | aq. (susp) | + |  |  |
| Corn oil | 100 | + | 1 |  | Arsenic Acid | aq. 80 | + | + |  |
| Animal oil | 100 | + | 1 |  |  | aq. dil. | + | + |  |
| Vegetable oil | 100 | + | 1 |  | Benzoic acid | 100 | + | + |  |
| Olive oil | 100 | + | + | + |  | aq. any | + | + | + |
| Palm kernel oil |  | + | 1 |  | Boric acid | 100 | + | + | + |
| Silicone oil | 100 | + | + | + |  | aq. stat old | + | + | + |
| Soybean oil | 100 | + | 1 |  | Bromhydric acid | conc. | + |  |  |
| Vaseline oil |  | + | 1 | - | Bromic acid | conc. | + |  |  |
| Fine spindle oil | 100 | + | - |  | Butyric acid | aq. 20 | + |  |  |
| Transformer oil | 100 | + | 1 |  |  | 100 | + |  |  |
| Lubricating oils | 100 | 1 |  |  | Citric acid | aq. any | + | + | + |
| Mineral oils (without aromatic components) | 100 | + | 1 | - | Hydrochloric acid | 36 10 | + + |  | + |
| Machine oils | 100 | + | 1 | - | Chloric acid | aq. 1 | + | 1 | - |
| Engine oils | 100 | + | 1 | - | Chloraacetic acid | (di) 100 | + | 1 |  |
| Acetaldehyde | 100 | 1 | - |  |  | (mono) 100 | + | + |  |
|  | a. 40 | + | + |  |  | (tri) 100 | + | + |  |
| Ammonium acetate | aq. any | + | + | + | Chlorosulfuric acid | 100 | - | - | - |
| Amyl acetate | 100 | 1 | - |  | Chromic acid | 50 | + | + |  |
| Butyl acetate | 100 | 1 | - | - |  | 20 | + | + |  |
| Ethyl acetate | 100 | + | 1 |  | Diglycolic acid | a. 30 | + | + |  |
| Methyl acetate | 100 | + | +e |  |  | aq. stt cold | + |  |  |
| Lead acetate | aq. stat ocld | + | + |  | Stearic acid | 100 | + | 1 |  |
| Vinyl acetate | 100 | + | 1 |  | Hydrofluoric acid | 70 | + |  |  |
| Sodium acetate | aq. stat ocld | + | + | + |  | 40 | + | + |  |
| Acetophenone | 100 | + | 1 |  |  |  |  |  |  |
| Acetone | 100 | + | +e |  |  |  |  |  |  |
| Acetic acid (glacial) | 100 | + | , | - |  |  |  |  |  |


| Product | concent | temperature |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | \% | $20^{\circ}$ | arc | 1000 |
| Formic acid | 100 | + | 1 |  |
|  | a. 85 | + | 1 |  |
|  | a. 50 | + | 1 |  |
|  | a. $2 \mathrm{n}(-9)$ | + | + |  |
| Phosphoric acid | 85 | + | + | + |
|  | 60 | + | + |  |
|  | up to 30 | + | + |  |
| Phthalic acid | a. 50 | + | + |  |
| Glycolic acid | 100 | + |  |  |
| Palm kernel fatty acid | 100 | 1 |  |  |
| Lactic acid | a. 90 | + | + | + |
|  | a. 50 | + | + | + |
|  | a. 20 | + | + | + |
|  | a. 10 | + | + | + |
| Maleic acid | 100 | + | + |  |
|  | aq, sat. cold | + | + |  |
| Malic acid | aq, sat. cold | + | + |  |
| Nitric acid | 68 | - | - |  |
|  | 50 | 1 | - |  |
|  | up to 30 | + | 1 |  |
| Oleic acid | 100 | + | 1 | - |
| Oxalic acid | a. 50 | + | 1 |  |
|  | a. 30 | + | + | + |
|  | aq, stat cold | + | 1 |  |
| Perchloric acid | a. 2 n | + | + |  |
| Picric acid | 1 | + |  |  |
| Propionic acid | a. 50 | + | + |  |
| Prussic acid | aq. any | + | + |  |
| Silichofluoric acid | a. . 41032 | + |  |  |
| Succinic acid | 100 | + | + |  |
|  | aq, sat cold | + | + |  |
| Sulphuric acid | 98 | 1 | - |  |
|  | 85 | + | 1 |  |
|  | 50 | + | + |  |
|  | 10 | + | + | + |
| Fatty acids (C6) | 100 | + | + |  |
| Tartaric acid | a. 10 | + | + |  |
|  | aq, stat cold | + | + |  |
| Acrylonitrile | 100 | + |  |  |
| Dinonyl adipate | 100 | + |  |  |
| Dioctyl adipate | 100 | + |  |  |
| Water (drinking, dest.) |  | + | + | + |
| Bromine water | cold sat. | - | - | - |
| Chlorine water | cold sat. | 1 | - |  |


| Product | concent. | temprature |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | \% | $20 . \mathrm{C}$ | Soc | 1000 |
| Sea water |  | + | + | + |
| Soda water |  | + | + |  |
| Mineral water |  | + | + | + |
| Hydrogen peroxide | 30 | + | 1 |  |
|  | 10 | + | + |  |
|  | 4 | + | + |  |
| Aqua regia |  | 1 | - |  |
| Camphor | 100 | + |  |  |
| Ally alcohol | 96 | + | + |  |
| Amyl alcohol | 100 | + | + | + |
| Benzyl alcohol | 100 | + | 1 |  |
| Wax alcohol | 100 | 1 | - |  |
| Copra alcohol | 100 | + | 1 |  |
| Ethyl alcohol | 100 | + |  |  |
|  | 96 | + | + | + |
| Ethyl alcohol (in fermentation) | usual | + |  |  |
| Ethyl alcohol + acetic acid (in fermentation) | usual | + |  |  |
| Furfuryl alcohol | 100 | + | 1 |  |
| Methoxybutyl alcohol | 100 | + |  |  |
| Proparty alcohol | a. 7 | + | + |  |
| Starch | 100 | + | + |  |
|  | ins salution | + | + |  |
| Tar |  | + | 1 |  |
| Alum (of all kinds) |  | + | + |  |
| Ammonia | a. 30 | + | + |  |
|  | a. 15 | + |  |  |
|  | a. 10 | + | + |  |
|  | smoses | + | + |  |
|  | Hiquid 100 | + |  |  |
| Acetic anhydride | 100 | + | 1 | - |
| Sulphur dioxide | any | + | + | + |
| Aniline | 100 | + | + |  |
| Anisole |  | 1 | 1 |  |
| Antifreeze |  | + | + | + |
| Antiformin (benzaldoxime) | a. 2 | + | + |  |
| Salted herring |  | + |  |  |
| Rum aroma |  | + |  |  |
| Asphalt |  | + | 1 |  |
| Aspirin |  | + |  |  |
| Sugar (dry) | 100 | + | + | + |
| Sugar (in solution) | aq. any | + | + | + |
| Sulphur | 100 | + | + | + |
| Chrome baths |  | $+$ | + |  |


| Product | concent. | temprature |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | \% | 200 | 600 | 1000 |
| Benzene | 100 | 1 | - |  |
| Benzaldehyde | 100 | + |  |  |
|  | aq. st. cold | + |  |  |
| Sodium benzoate | aq, st. cold | + | + |  |
| Carbon dioxide | (wet) any | + | + |  |
|  | (dry) 100 | + | + |  |
| Sodium bisulfite | aq. st. cold | + | + |  |
| Moth balls |  | + |  |  |
| Potassium borate | aq. 1 | + | + |  |
| Borax | aq. st. cold | + | + | + |
| Potassium bromate | aq. st. cold | + | + | + |
| Bromine | (liquid) 100 | - |  |  |
|  | (mpous) Himb | - | - |  |
|  | (spanas iom | 1 | - |  |
| Potassium bromide | aq. statcold | + | + | + |
| Butadiene | 100 | 1 | - |  |
| Butane | (sames) 100 | + | + |  |
|  | (liquid) 100 | + |  |  |
| Butanediol | a. 100 | + | + |  |
| Butanol | 100 | + | 1 | 1 |
| Butanetriol | a. 100 | + | + |  |
| Butylphenol | cold sat. | + |  |  |
| Butylphenone | 100 | - |  |  |
| Butylglycol | 100 | + |  |  |
| Butynediol | 100 | + |  |  |
| Butyraldehyde | 100 | 1 |  |  |
| Butoxyl |  | + |  |  |
| Cocoa | ready to be consumed | + | + | + |
|  | powder | + |  |  |
| Coffee | eady to be consumed | + | + | + |
|  | grimangemad | + |  |  |
| Cinnamon |  | + |  |  |
| Sodium hydrogencarbonate (sodium bicarbonate) | aq. stat cold | + | + | + |
| Ammonium carbonate | aq. any | + | + | + |
| Calcium carbonate | aq, stat cold | + | + | + |
| Potassium carbonate | aq. st. cold | + | + |  |
| Sodium carbonate | a. 10 | + | + | + |
|  | aq. st.cold | + | + |  |
| Beeswax |  | + | 1 |  |
| Encaustic wax | 100 | + | 1 |  |
| Beer |  | + |  |  |
| Potassium cyanide | 100 | + |  |  |
|  | aq. st. cold | + | + |  |


| Product | concent | temprature |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | \% | $2{ }^{20} \mathrm{C}$ | com | 1000 |
| Cyclohexane | 100 | + |  |  |
| Cyclohexanol | 100 | + | 1 |  |
| Cyclohexanone | 100 | + | 1 |  |
| Clophenes |  | + | / | - |
| Chloramine | aq. any | + |  |  |
| Potassium chlorate | aq. statold | + | + | + |
| Sodium chlorate | aq. st. ocold | + | + |  |
| Aniline hydrochloride | sat. a. | + | + |  |
| Phenylhydrazine hydrochloride | a. | + | 1 |  |
| Sodium chlorite | sat. a. | + | 1 |  |
| Chlorine | $\begin{gathered} \text { gaseeuss } \\ \text { dryy } 100 \end{gathered}$ | - |  |  |
|  | $\begin{aligned} & \text { gaseous, } \\ & \text { wet } 10 \end{aligned}$ | 1 |  |  |
|  | Higutid 100 | - |  |  |
| Chlorobenzene | 100 | + |  |  |
| Chloroethanol | 100 | + | + |  |
| Chloroform | 100 | / | - |  |
| Ammonium chloride | aq. any | + | + | + |
| Antimony chloride | a. 90 | + |  |  |
| Benzoyl chloride | 100 | 1 |  |  |
| Lime chloride | aqueous | + | + |  |
| Calcium chloride | a. 50 | + | + | + |
|  | a. 10 | + | + | + |
|  | aq. stat old | + | + | + |
| Ethyl chloride | 100 | 1 |  |  |
| Ethylene chloride | 100 | 1 |  |  |
| Hydrogen chloride (gaseous, dry and wet) | any | + | + |  |
| Methylene chloride | 100 | 1 | - e |  |
| Methyl chloride | 100 | 1 | - |  |
| Sulphuryl chloride | 100 | - |  |  |
| Thionyl chloride | 100 | - |  |  |
| Tricyanogen chloride | 100 | + |  |  |
| Stannous chloride | aq. st. cold | + | + |  |
| Potassium chloride | 100 | + | + | + |
| Sodium chloride | aq. stat.old | + | + | + |
|  | a. 10 | + | + | + |
|  | a. 50 | + |  |  |
| Coca-Cola |  | + |  |  |
| Calendering glue |  | + | + |  |
| Apple compote |  | + | + | + |
| Cognac |  | + |  |  |
| Shoe polish |  | + | 1 |  |
| Cresols | 100 | + | 1 |  |
|  | insolution | + |  |  |


| Product | concent | temprature |  |  | Product |  | temperature |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | \% | 20.0 | arc | ${ }^{100 C}$ |  |  | ${ }^{200}$ | 600 | 100C |
| Potassium chromate | a. 40 | + | + | + | Cellulose tanning extracts | usual | + |  |  |
| Crotonaldehyde | 100 | + |  |  | Vegetable tanning extracts | usual | + |  |  |
| CY3 (machine oil) |  | + | 1 | - | Phenol | hotasta. | + | + |  |
| Shampoo |  | + | + |  |  | comerc. | + | + |  |
| Sauerkraut (ready to be served) |  | + | + | + | Fluorine (dry) | 100 | - |  |  |
| Decalin | 100 | 1 | 1 |  | Ammonium fluoride | a. up to 20 | + | + |  |
| Dextrin | aq. stitold | + |  |  | Formaldehyde | a. $30 / 40$ | + | + |  |
| Dichlorobenzene | 100 | 1 |  |  |  | a. 10 | + | + |  |
| Dichloroethane | 100 | + |  |  | Ammonium phosphate | aq. any | + | + | + |
| Dichloroethylene | 100 | + |  |  | Tricesyl phosphate | 100 | + | 1 |  |
| Potassium dichromate | aq. st. cold | + | + | + | Trioctyl phosphate |  | + |  |  |
| Diethanolamine | 100 | + |  |  | Sodium phosphates | hotata. | + | + | + |
| Diisobutylketone | 100 | + | - |  | Phosgene | 100 | 1 | 1 |  |
| Dimethylamine | 100 | + |  |  | Frigen 113 | 100 | - |  |  |
| Dimethylformamide | 100 | + | + |  | Fructose |  | + | + | + |
| Dioxane | 100 | 1 | 1 | - | Butyl phthalate | 100 | + | 1 | 1 |
| Light DTE (turbine oil) |  | - | - |  | Dibutyl phthalate | 100 | + | 1 | 1 |
| Cold cuts |  | + | + |  | Dihexyl phthalate | 100 | + | 1 |  |
| False fir needles essence | 100 | + | + |  | Dinonyl phthalate | 100 | + |  |  |
| Wild spruce needles essence |  | + | + |  | Dioctyl phthalate | 100 | + |  |  |
| Bitter almonds essence |  | + |  |  | Fuel oils | 100 | + | 1 |  |
| Carnation essence |  | + | 1 |  | Roasting gas (dry) Lighting gas (benzene free) | any | + |  |  |
| Lemon rind essence |  | + |  |  | Lighting gas (benzene free) |  | $+$ |  |  |
| Orange peel essence |  | + |  |  | Diesel | 100 | 1 |  |  |
| Lemon essence |  | + |  |  | Crude petrol | 100 | 1 |  |  |
| Mint essence |  | + |  |  | Normal petrol | 100 | 1 |  |  |
| Nail polish |  | + | 1 |  | Super petrol | 100 | 1 | - |  |
| Yeast spices |  | + | + |  | Petrol boiling point $100-140^{\circ} \mathrm{C}$ | 100 | 1 | - |  |
| Whale sperm |  | + |  |  | Gelatine | aq. any | + | + |  |
| Amylacetic ester | 100 | 1 | - |  | Gin |  | + |  |  |
| Butylacetic ester | 100 | 1 | - |  | Glycerine. | 100 | + | + | + |
| Monoloracetic acid ethyl ester | 100 | + | + |  |  | aq. any | + | + | + |
| Methylacetic ester | 100 | + | +e |  | Glycocole | a. 10 | + |  |  |
| Dichloroacetic acid methyl ester | 100 | + | + |  | Glycol | 100 | + | + | + |
| Monochloracetic acid methyl ester | 100 | + | + |  |  | any | + | + | + |
| Isopropyl ester | 100 | 1 | - |  | Glucose | hotstata | + | + | + |
| Petroleum ester | 100 | + | 1 |  | Glucose (grape sugar) | hotata | + | + |  |
| Dibutyl ether | 100 | 1 | - |  | Flour | 100 | + |  |  |
| Ethyl ether | 100 | 1 |  |  | Heptane | 100 | 1 | 1 |  |
| Ethylbenzene | 100 | 1 | - |  | Hexane | 100 | + | 1 |  |
| Ethylene glycol | 100 | + | + | + | Hexanetriol | 100 | + | + | + |
| Acetic ester | 100 | + | 1 |  | Chloral hydrate | any | 1 | - |  |
| Ethylhexanol | 100 | + |  |  | Hydrazine hydrate |  | + |  |  |


| Product | concent | temprrature |  |  | Product | CONCENT. <br> \% | temprrature |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | \% | ${ }^{20 . C}$ | arc | 1000 |  |  | 200 | 6ra | 1000 |
| Hydrogen | 100 | + | + | - | Mixture of liquid paraffins 12-150E |  | + | 1 |  |
| Hydroquinone | 100 | + |  |  | Honey |  | + | + |  |
| Barium hydroxide | aq. any | + | + |  | Morpholine |  | + | + |  |
| Sodium hydroxide | 100 | + | + |  | Mustard |  | + |  |  |
| Calcium hypochlorite | aq. any | + | + |  | Mowilith D |  | + |  |  |
| Sodium hypochlorite | a. 20 | + | 1 |  | Naphthalene | 100 | + |  |  |
|  | a. 10 | + | + |  | Cream |  | + |  |  |
|  | a. 6 | + | + | + | Ammonium nitrate | aq. any | + | + | + |
| Isobutyric aldehyde | 100 | 1 |  |  | Calcium nitrate | a. 50 | + | + |  |
| Isooctane | 100 | + | 1 |  | Silver nitrate | a. 20 | + | + | + |
| Isopropanol | 100 | + | + | + | Potassium nitrate | 100 | + | + |  |
|  | aq. any | + | + |  |  | aq. stat old | + | + |  |
| Soap | liquid | + | + |  | Sodium nitrate | aq. statcold | + | + |  |
|  | bar | + | + |  | Nitrobenzene | 100 | + | T |  |
| Jelly |  | + | + | + | or Nitrotoluene |  | + | 1 |  |
| Tomato juice |  | + | + |  | Octylcresol | 100 | 1 | - |  |
| Tomato ketchup |  | + | + |  | Oleum | any | - | - | - |
| Lanolin (wool grease) |  | + | 1 |  | Urine |  | + | + |  |
| Milk |  | + | + | + | Phosphorus oxychloride | 100 | + | 1 |  |
| Pulses |  | + | + | + | Ethyl oxide | 100 | 1 e |  |  |
| Bisulphite bleach SO2 content | hotstat.a | + | + |  | Oxygen | any | + | 1 |  |
| Whitewash bleach, 12.5\% active chlorine |  | + | 1 | - | Ozone | 50 pphm | + | 1 |  |
| Yeast | aq. any | + |  |  | Sodium palmitate | 5 | + | + | + |
| Liqueurs |  | + |  |  | Paraffin | 100 | + | + |  |
| Brake fluid | 100 | + |  |  |  | Iiquid 100 | + | 1 | - |
| Lysol |  | + | 1 |  | Toothpastes |  | + | + |  |
| Fruit salad |  | + | - |  | Pectin | aq. stat cold | + | + |  |
| Mayonnaise |  | + |  |  | Phosphorus pentoxide | 100 | + |  |  |
| Pork lard |  | + | + | 1 | Sodium perborate | aq. statcold | + | + | + |
| Butter |  | + | + |  | Potassium perchlorate | a. 1 | + | + |  |
| Margarine |  | + | + |  | Perchlorethylene | 100 | 1 | - |  |
| Molasses | usual | + | + |  | Perfume |  | + |  |  |
| Beet molasses |  | + | + | + | Potassium permanganate | aq. st. cold | + | + |  |
| Menthol | 100 | + |  |  | Potassium persulphate | 100 | + |  |  |
| Mercury | 100 | + | + |  |  | aq. any | + | + |  |
| Jam |  | + | + | + | Fish | pickled | + | + | + |
| Methanol | 100 | + | +e |  | Petroleum | 100 | + | 1 |  |
|  | a. 50 | + | + |  | Paprika |  | + | + |  |
| Methylamine | 100 | + |  |  | Pepper |  | + | + |  |
|  | a. 32 | + |  |  | Pyridine | 100 | 1 | 1 |  |
| Methyl bromide | 100 | - | - |  | Caustic Potash | 55 | + | + | + |
| Methyl ethyl ketone | 100 | + | 1 |  |  | 25 | + | + | + |
| Chromic mixture |  | - | - |  |  | 2 n | + | + | + |
| Mixture of naphthene and liquid prafifin 8.5 . ${ }^{\text {F }}$ | 100 | + | 1 | - | Dairy products |  | + | + | + |


| Product | concent | temperature |  |  | Product | concent | temperature |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | \% | 200 | ¢00 | 1000 |  | \% | 20.4 | coc 100 | anc |
| Dishwashing products |  | + | + | + | Dimethyl sulphate | 100 | 1 | - |  |
| Propane | gsous 100 | + | + |  |  | a. 50 | 1 | 1 |  |
|  | liquid 100 | + |  |  | Hydrazine sulphate | 10 | + | + |  |
| i-Propanol +n -Propanol | 100 | + | + |  | Hydroxylamine sulphate | a. 12 | + | + |  |
| Propylene glycol | a. 100 | + | + |  | Potassium sulphate | aq. st. cold | + | + |  |
| Pudding |  | + | + | + | Sodium sulphate (Glauber salt) | aq. stat ocld | + | + |  |
| Furniture polish |  | + | 1 | - | Sodium sulphide | a. 40 | + | + |  |
| Kerosene | 100 | / | 1 |  |  | aq, stat old | + | + |  |
| Cheese |  | + |  |  | Fatty alcohol sulphanate |  | + | 1 |  |
| Quinine |  | + |  |  | Ammonium sulphide | aq. any | + | + |  |
| Nail polish remover |  | + | 1 |  | Carbon sulphide | 100 | + |  |  |
| Horseradish |  | + |  |  | Hydrogen sulphide | (dry) 100 | + | + |  |
| Cottage cheese |  | + |  |  |  | aq. any | + | + |  |
| Photographic developers | ready to be used | + |  |  | Tea | cosamption | + | + + | + |
|  | commectial | + | + |  |  | leaves | + | + |  |
| Rum |  | + | + |  | Tetrachloroethane | 100 | 1 | - |  |
| Sagrotan |  | + | 1 |  | Tetrachloroethylene | 100 | 1 | - |  |
| Common salt | aq. any | + | + |  | Carbon tetrachloride | 100 | - | - |  |
| Fertilizing salt | sat. a. | + | + |  | Tetraethyl lead | 100 | + |  |  |
| Fixing salt in solution | any | + | + |  | Tetrahydrofuran | 100 | 1 | - |  |
| Aluminium salts | aq. any | + | + | + | Tetrahydonaphthalene | 100 | - | - |  |
| Barium salts | aq. any | + | + | + | Ink |  | + | + |  |
| Zinc salts | aq. 9.tal cold | + | + |  | Tincture of iodine | usual | + |  |  |
| Copper salts | aq. 9 st cold | + | + |  | Thiophene | 100 | 1 | - |  |
| Chromium salts (bivalent and trivalent) | aq. stat cold | + | + |  | Sodium thiosulphate | aq. stat old | + | + |  |
| Iron salts | aq. stat cold | + | + | + | Toluene | 100 | 1 | - |  |
| Mercury salts | aq.ats cold | + | + |  | Turpentine | 100 | - | - - | - |
| Nickel salts | aq. 9tat oold | + | + |  | Trichloroethylene | 100 | 1 | 1 |  |
| Silver salts | aq. stat old | + | + |  | Antimony trichloride | 100 | + | + |  |
| Magnesium salts | aq. 9 at cold | + | + | + | Phosphorus trichloride | 100 | + |  |  |
| Dibutyl sebacate | 100 | + |  |  | Trielanolamine | 100 | + |  |  |
| Beef tallow | 100 | + | + |  | Urea | aq. stat old | + | + |  |
|  | sulphur emission | + |  |  | Vanilla |  | + | + |  |
| Shell-Dromus | a. 0,5 | + | 1 | 1 | Nitrous vapours | conc. | + | - - | - |
| Soluble silicate |  | + | + |  | Vaseline |  | + | 1 |  |
| Silicone emulsion |  | + | + | + | Wine |  | + | + |  |
| Viscose solution for spinning |  | + | + |  | Whisky |  | + |  |  |
| Soap solution | any | + | + |  | White spirit | 100 | 1 | - |  |
| Iodine solution | 50 | + | + |  | p-Xylene | 100 | - | - |  |
| Caustic soda | 52 | + | + | + | Potassium iodide | aq. stat ocld | + | + |  |
|  | 30 | + | + | + | Lemon juice |  | + | + |  |
|  | 2 n | + | + | + | Apple juice |  | + | + |  |
| Fat-free buttermilk |  | + |  |  | American pineapple juice |  | + | + |  |
| Ammonium sulphate | aq. any | + | + | + | Fruit juice |  | + | + + | + |

Material properties
What is Poliethylene. Types of poliethylene 10.1 Physico-chemical properties 10.2 Gas permeability of PE pipes 10.3 Chemical resistance 10.4 Bacterial resistance 10.5

Product range
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## 11

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Flanged systems 14.4
$\begin{array}{ll}\text { Mechanged systems } & 14.4 \\ \text { Mystems } & 14.5\end{array}$ Installation of branch systems $\quad 14.6$

Annex


Polyethylene is a polymer made up of ethylene monomers which, depending on the polymerisation process used, are arranged into chains that may be more or less intertwined and more or less long. Their length and this intertwining will define the properties it will have.

When cooled, polymer chains can be arranged into crystalline structures (crystallisation) or maintain the disordered "ball" structure (amorphous structure). Depending on the grade of each of these structures, polyethylenes of different densities are obtained:

Low-density polyethylene: Density between $0.915-0.930 \mathrm{~g} / \mathrm{cm} 3$ and a degree of crystallinity of $40 \%$ to $55 \%$. It is also called high pressure, because it is obtained in reactors that work at high pressures (up to 1000 atm . They have very branched molecules.

Medium-density polyethylene: Density between $0.930-0.940 \mathrm{~g} / \mathrm{cm} 3$ and a degree of crystallinity between 50 and $60 \%$. Molecules with little branching.

High-density polyethylene: Density between $0.940-0.965 \mathrm{~g} / \mathrm{cm} 3$ and a crystallinity degree of $60-80 \%$. It is also called low pressure because it is obtained in reactors that work at a much lower pressure than the previous ones (from 30 to 40 atm ). Molecules with short branches.

The properties of polyethylene depend mainly on density, molecular weight (length of chains) and molecular weight distribution.

The REPOLEN system uses high-density polyethylene, PE-100, with a bimodal distribution of molecular weights.

### 10.2 PHYSICO-CHEMICAL PROPERTIES

The higher the percentage of crystallinity, the higher: Tensile strength; modulus of elasticity (rigidity); hardness; resistance to solvents; impermeability to gases and vapours, etc. On the contrary, the lower: Impact resistance; translucency; and stress cracking. On the other hand, the higher the molecular weight, the higher the tensile strength and internal pressure, but the lower the fluidity of the melt. In summary, the most important properties of the PE-100 used to manufacture REPOLEN pipes and fittings are.

| PROPERTY | VALUE | UNITS | TEST PROCEDURE |
| :--- | :---: | :---: | :---: |
| Fluidity index $\left(190^{\circ} \mathrm{C} ; 21.6 \mathrm{~kg}\right)$ | 7 | $\mathrm{~g} / 10 \mathrm{~min}$ | ISO 1133 |
| Fluidity index $\left(190^{\circ} \mathrm{C} ; 5 \mathrm{~kg}\right)$ | 0.27 | $\mathrm{~g} / 10 \mathrm{~min}$ | ISO 1133 |
| Density at $233^{\circ} \mathrm{C}$ | 962 | $\mathrm{Kg} / \mathrm{m} 3$ | ISO 1183 |
| Tensile strength at the breaking point | 38 | MPa | ISO $527-2$ |
| Elongation at the breaking point | $>600$ | $\%$ | ISO $527-2$ |
| Elastic Flexural Modulus | 1000 | MPa | ISO 178 |
| Oxidation induction time $\left(210^{\circ} \mathrm{C}\right)$ | $>20$ | Min | UNE EN 728 |
| VICAT softening temperaure $(10 \mathrm{~N})$ | 128 | ${ }^{\circ} \mathrm{C}$ | ISO 306 |
| Long-term hydrostatic resistance after 50 years and $20^{\circ} \mathrm{C}(97.5 \% \mathrm{LCL})$, MRS | $>10.0$ | MPa | ISO TR 9080 |



Due to their molecular structure they have excellent resistance to a great variety of chemical agents. In the same way, they feature a very good resistance to electrochemical corrosions, due to the effect of sea water; urban and industrial discharges, etc.

For further information, please refer to Annex I.

## BACTERIAL RESISTANCE 10.5

Due to their characteristics, PE pipes do not favour the cultivation of any type of microorganism, bacteria or known fungus. The mirror finish also helps prevent the formation of fouling that can become a very suitable medium for the appearance of undesirable organisms.

The coefficient of permeability depends on the type of plastic and gas. Polyethylene is also influenced by its basic density. In the table the values of

## P (cm3 / m bar)

| Gas | $\mathrm{P}(\mathrm{cm} 3 / \mathrm{m}$ bar $)$ |
| :--- | :---: |
| Nitrogen | 0.018 |
| Air | 0.029 |
| Carbon Monoxide | 0.036 |
| Natural Gas | 0.056 |
| Methane | 0.056 |
| Argon | 0.066 |
| Oxygen | 0.072 |
| Ethane | 0.089 |
| Helium | 0.15 |
| Hydrogen | 0.22 |
| Carbon Dioxide | 0.28 |
| Sulphur Dioxide | 0.43 | these coefficients for the most used gases can be seen on the table.


| Gas | $\mathrm{P}(\mathrm{cm} 3 / \mathrm{m}$ bar) |
| :--- | :---: |
| Nitrogen | 0.018 |
| Air | 0.029 |
| Carbon Monoxide | 0.036 |
| Natural Gas | 0.056 |
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| Oxygen | 0.072 |
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| Helium | 0.15 |
| Hydrogen | 0.22 |
| Carbon Dioxide | 0.28 |
| Sulphur Dioxide | 0.43 |

$\qquad$ -


PRODUCI


RANGE
11.1 PE-100 pipes UNE-EN 12201

- Human consumption - Reclaimed water
$\rightarrow$ Sewerg
11.2 PE-100 Pipes UNE-EN 15501 (Gas)
11.3 PE-100 pipes Cables, electricity and telecommunications
11.4 Thermofusion fittings
11.5 Electroweldable fittings and transitions
11.6 Compression fittings
11.1 PE-100 pipes UNE-EN 12201

For human consumption water: Black with blue stripes
For reclaimed water: Black with purple stripes
For sewerage, sanitation and other applications: Black with brown stripes
Calculated with a safety coefficient $\mathrm{C}=1.25$


S5 SDR11 PN16

|  | S5 SDR11 PN16 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Nominal diameter $(\mathrm{mm})$ | Intemal diameter $(\mathrm{mm})$ | Thickess $(\mathrm{mm})$ | Weght (kg/m) | Capacit (l/m) |
| 20 | 16 | $2-2.3$ | 0,11 | 0,2 |
| 25 | 20.4 | $2.3-2.7$ | 0,17 | 0,33 |
| 32 | 26 | $3-3.4$ | 0,28 | 0,53 |
| 40 | 32.6 | $3.7-4.2$ | 0.42 | 0.83 |
| 50 | 40.8 | $4.6-5.2$ | 0,66 | 1,31 |
| 63 | 51.4 | $5.8-6.5$ | 1,02 | 2,07 |
| 75 | 61.4 | $6.8-7.6$ | 1,46 | 2,96 |
| 90 | 73.6 | $8.2-9.2$ | 2,1 | 4,25 |
| 110 | 90 | $10-11.1$ | 3,14 | 6,36 |
| 125 | 102.2 | $11.4-12.7$ | 4,13 | 8,2 |
| 140 | 114.6 | $12.7-14.1$ | 5,14 | 10,31 |
| 160 | 130.8 | $14.6-16.2$ | 6,75 | 13,44 |


| S4 SDR9 PN20 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Nominal diameter (mm) | Internal diameter (mm) | Thickness (mm) | Veight (kg/m) | Capacity (1/m) |
| 20 | 15.4 | 2.3-2.7 | 0,14 | 0,19 |
| 25 | 19 | 3-3.4 | 0,21 | 0,28 |
| 32 | 24.8 | 3.6-4.1 | 0,33 | 0,48 |
| 40 | 31 | 4.5-5.1 | 0,51 | 0,75 |
| 50 | 38.8 | 5.6-6.3 | 0,79 | 1,18 |
| 63 | 48.8 | 7.1-8 | 1,27 | 1,87 |
| 75 | 58.2 | $8.4-9.4$ | 1,75 | 2,66 |
| 90 | 69.8 | 0.1 - 11.3 | 2,52 | 3,83 |
| 110 | 85.4 | 12.3-13.7 | 3,74 | 5,73 |

### 11.4 FITTINGS

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|  | 3 Cam | (c) |
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(c)


SYSTEM
$\square$ Le

- Easy handling and installation, thanks in part to its reduced weigh

Low maintenance cost.
Multiple connection systems.
$100 \%$ recyclable
Resistant to high energy radiation.
Ultraviolet protection. Suitable for outdoor use
Highly resistant to abrasion.

- Absorbs vibrations and ground movements (Seismic hazards). Also passage of heavy vehicles.
- Ele
alvanic currents.
- 

nternal mirror shine and very low roughness coefficient
Minimal pressure drop.
Highly corrosion resistant
High chemical resistance to both acids and alkali
$100 \%$ non-toxic.
Very low noise transmission leve.
Flexibility. Possibility of cold bending.
High impermeability to gases.
Low celerity (wave propagation velocity)
High resistance to temperatures below $0^{\circ} \mathrm{C}$.


Drinking water pipes


Recycled waters



| PROPERTY OF THE PIPE | VALUE | UNITS |  |
| :--- | :---: | :---: | :---: |
| Lineal thermal expansion coefficient | 0.22 | $\mathrm{~mm} / \mathrm{m}{ }^{\circ} \mathrm{C}$ |  |
| Thermal conductivity | 0.37 | $\mathrm{Kcal} / \mathrm{m}{ }^{\circ} \mathrm{C}$ |  |
| Poisson coefficient | 0.4 | o |  |
| Dielectric constant | k | 2.5 | $-\mathrm{-}$ |
| Hydraulic roughness | k |  |  |
|  | N (Manning) | 0.003 | mm |
|  | C (Hazen-Williams) | 0.008 | --- |
| Shore D hardness |  | 150 | --- |
| Carbon black content | 65 | -- |  |
| Carbon black dispersion | $2-2.5$ | mass |  |
| Volatile substances content | $<3$ | -- |  |
| Water content | $<350$ | $\mathrm{mg} / \mathrm{kg}$ |  |

12.3 MARKING AND TRACEABILITY

The marking of the pipes is done in accordance with the UNE EN 12201 standard and the requirements of the AENOR Special Regulations, RP.001.01. in the case of water, and the UNE EN 1555 standard and the AENOR Special Regulations RP. 001.05 in the case of gaseous fuels. The purpose of pipe marking is to provide the necessary information to the installer, the user and the manufacturer, if necessary. The marking includes:

- Trademark: REPOLEN
- Reference to the AENOR mark (Product Certificate) and contract number.
- Material it is made of.
- Nominal diameter and thickness.
- Nominal pressure and SDR.
- Intended use: W for drinking water; P for pressurised sewage and sewerage; W/P for mixed use; and GAS for gaseous fuels.

Manufacturing period

- Symbol of suitability for food use, if applicable.
- Reference to $100 \%$ national manufacture.

The manufacturing period is unique for each pipe production, enabling complete traceability of the finished product. Knowing this number, it is possible to make a complete tracking from the entry of raw material, until the delivery at our clients' home.

Although the most used reference is the nominal pressure (PN), it is convenient to know the SDR and the S:

- SDR is the relation between the outer diameter and the thickness of the pipe, according to the equation:

$$
\text { SDR }=\varphi \text { ext / thickness }
$$

- $S$ is a dimensionless number that classifies the piping according to ISO 4065 standard and indicates the relationship between the tangential tension $(\sigma)$ and the working pressure (P) at a certain temperature, according:


## $S=\sigma / P$

STORAGE, HANDLING AND TRANSPORT
12.4

PE pipes can be stored indoors or outdoors, thanks to the protection against solar radiation given by the carbon black.
The rolls can be stored horizontally on top of each other up to a height of 1.5 m and vertically only one height.
The bars can be stacked on flat and clean horizontal surfaces, having the necessary supports to prevent deformation and up to a maximum height of 1.5 m .

PE-100 pipes must be stored in such a way that they cannot come into contact with fuels, solvents, aggressive paints, etc. It is also advisable to avoid contact or proximity to surfaces that can reach $50^{\circ} \mathrm{C}$ or more
PE-100 is a resistant and flexible material, but it is necessary to avoid dragging on rough surfaces and contact with sharp-edged objects.


If, for any reason, a pipe with a damaged piece or with bends is detected, the damaged piece must be removed before installation

For transport, it is important to do it on a horizontal plane free of nails or protrusions that could damage the piping. Care must be taken in the correct stacking of the pipes. Do not place heavy loads on top that could deform the pipes.

When getting them off the lorry, they should NEVER be thrown, but accompany them when unloading and subsequent stacking

$\boldsymbol{\otimes}$

$\boldsymbol{\otimes}$

## 13.1 buried Installations

In general, the following can be established:

- Polyethylene pipings are flexible, susceptible to permanent deformation due to the load and the time of application of the load. These deformations shall be limited by applying the corresponding calculations (UNE 53-331).
- If there are steep slopes in the route, pipe laying should preferably be carried out in the ascending direction, having anchorage points in mind.
When pipe laying has to be interrupted, the ends should be plugged
to prevent the ingress of foreign bodies.
If there is a risk of flooding of the trench, points of attachment of the piping to the bed should be provided to prevent it from floating and to maintain the layout.
-The layout must follow a meandering path

Buried installation techniques can be: With conventional trenches, plough with mole drain and push plough. For trenching, a series of factors must be taken into account:
$\square$ Trench width
This obviously depends on the diameter of the piping, the depth of the trench and the type of soil. There should be enough space on both sides of the pipe to facilitate compaction of the filling, such as:

| DN $(\mathrm{mm})$ | Minimum trench width $(\mathrm{OD}+\mathrm{x})$, meters |  |  |
| :--- | :---: | :---: | :---: |
|  | Piped trench | Trench without shoring |  |
|  |  | $\beta>60^{\circ}$ | $\beta<60^{\circ}$ |
| 225 | $\mathrm{OD}+0.40$ | $\mathrm{OD}+0.40$ |  |
| $225<\mathrm{DN}<350$ | $\mathrm{OD}+0.5$ | $\mathrm{OD}+0.50$ | $\mathrm{OD}+0.40$ |
| $350<\mathrm{DN}<700$ | $\mathrm{OD}+0.70$ | $\mathrm{OD}+0.70$ | $\mathrm{OD}+0.40$ |
| $700<\mathrm{DN}<1200$ | $\mathrm{OD}+0.85$ | $\mathrm{OD}+0.85$ | $\mathrm{OD}+0.40$ |
| $\mathrm{DN}>1200$ | $\mathrm{OD}+1.0$ | $\mathrm{OD}+1.0$ | $\mathrm{OD}+0.40$ |

## $\square$ Bed

If the terrain is even, it will be excavated to the ground level. If stones, foundations, rocks, etc. remain uncovered, they must be excavated below ground level for later filling of the bed. This additional excavation can be from 15 to 30 cm , and its filling will be done with the contribution of soil from the excavation, which is easily compactable and free of stones, or with loose sand.

■ Types of support
Two types of supports are considered:

- Type A Support: Consists of a continuous bed of compacted granular material on which the pipe rests. It must be evenly compacted across its entire length and wrap the pipe according to a $2 \alpha$ support angle, recommended $120^{\circ}$.
- Type B support: The pipe rests directly on the bottom of the trench or on the natural ground in the case of an installation under embankment. To be used only on sandy grounds free from lumps and stones.

Trench depth
It must protect the pipes from the loads they have to support, both fixed and mobile. To calculate these overloads, the information included in UNE 53331 IN standard must be taken into account. But as a general rule, the following is acceptable:


## Fill

The filling is carried out once the piping has been laid and tested. It must be calculated and carried out in such a way as to limit the deformation of the pipe. For this purpose, the material used must be chosen taking into account the mechanical criteria of resistance to loads, stability in its conditions of use, ease of installation and subsequent compaction.
this is not possible, it is recommended to make a section like the one in the following drawing, bearing in mind hat the upper generatrix of the pipe walls.



## Compacting

The compaction of the filler will depend on: The soil characteristics, the soil cover, the life time of the installation and the water table. The compaction equipment used will depend on the type of filling to be compacted.
The filling will be made by 10 cm successive layers, if possible with soil free of stones from the excavation itself, up to 30 cm the pipe generator getting $95 \%$ of the Normal Proctor in compaction. Care must be taken to balance the compaction on both sides of the pipe as to equalise the pressure on it. The rest of the filling can be done mechanically and with unsorted soil from the excavation.
13.2 NON-BURIED INSTALLATIONS

In non-buried installations it is very important to take into account issues such as lineal expansion, since the deformations that the pipe may undergo will be visible, causing a snaking effect that may lead to misunderstandings regarding the strength of the pipe.

The lineal expansion coefficient of polyethylene is considered to be 0.2 $\mathrm{mm} / \mathrm{m}^{\circ} \mathrm{C}$ for practical purposes. There are several formulas according to ENV 12108. The calculation equation is as follows:
$\Delta L$ is the increase in length that the pipe will have due to the lineal expansion, in millimetres.
L is the length of the pipe on which the lineal expansion is calculated in metres
$\lambda$ is the lineal expansion coefficient, in $\mathrm{mm} / \mathrm{m}^{\circ} \mathrm{C}$. $\Delta T$, is the temperature difference between the transported fluid and the ambient temperature

| $\lambda=0,2 \mathrm{~mm} / \mathrm{m}^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Piping } \\ \text { length }(\mathrm{m}) \end{gathered}$ | Lineal expansion of REPOLEN PE-100 piping $\Delta \mathrm{I}$ (mm) <br> Temperature difference $\Delta$ Tee ( ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |
|  | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 |
| 0.1 | 0.2 | 0.4 | 0.6 | 0.8 | 1 | 1.2 | 1.4 | 1.6 |
| 0.2 | 0.4 | 0.8 | 1.2 | 1.6 | 2 | 2.4 | 2.8 | 3.2 |
| 0.3 | 0.6 | 1.2 | 1.8 | 2.4 | 3 | 3.6 | 4.2 | 4.8 |
| 0.4 | 0.8 | 1.6 | 2.4 | 3.2 | 4 | 4.8 | 5.6 | 6.4 |
| 0.5 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| 0.6 | 1.2 | 2.4 | 3.6 | 4.8 | 6 | 7.2 | 8.4 | 9.6 |
| 0.7 | 1.4 | 2.8 | 4.2 | 5.6 | 7 | 8.4 | 9.8 | 11.2 |
| 0.8 | 1.6 | 3.2 | 4.8 | 6.4 | 8 | 9.6 | 11.2 | 12.8 |
| 0.9 | 4.8 | 3.6 | 5.4 | 7.2 | 9 | 10.8 | 12.6 | 14.4 |
| 1 | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 16 |
| 2 | 4 | 8 | 12 | 16 | 20 | 24 | 28 | 32 |
| 3 | 6 | 12 | 18 | 24 | 30 | 36 | 42 | 48 |
| 4 | 8 | 16 | 24 | 32 | 40 | 48 | 56 | 64 |
| 5 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 |
| 6 | 12 | 24 | 36 | 48 | 60 | 72 | 84 | 96 |
| 7 | 14 | 28 | 42 | 56 | 70 | 84 | 98 | 112 |
| 8 | 16 | 32 | 48 | 64 | 80 | 96 | 112 | 128 |
| 9 | 18 | 36 | 54 | 72 | 90 | 108 | 126 | 144 |
| 10 | 20 | 40 | 60 | 80 | 100 | 120 | 140 | 160 |

Among the compensation systems employed, are: - Compensators. There are different types of compensators on the market.

- Address changes: in "L", "Z" or "U".


The equations used for the calculation are:
$\mathrm{L}_{\mathrm{b} 1}=\sqrt{\frac{3 * \mathrm{DN} * \Delta \mathrm{~L} 1 * \mathrm{E}_{50}}{0.15 * \sigma_{\mathrm{s}}}}$
$\mathrm{L}_{\mathrm{b} 2}=\sqrt{\frac{3 * \mathrm{DN} * \Delta \mathrm{~L}_{\mathrm{b}} * \mathrm{E}_{50}}{0.15 * \sigma_{\mathrm{s}}}}$
$\mathrm{L}_{\mathrm{b}_{1}} y \mathrm{~L}_{\mathrm{b}_{2}}$ can be seen in the drawings. DN is the nominal diameter of the pipe, in mm. $\Delta L_{1}$ is the increase in length of the $L_{p}$, in mm. $\mathrm{E}_{50}$ is the long term modulus of elasticity at $20^{\circ} \mathrm{C}\left(\mathrm{E}_{50}=150 \mathrm{~N} / \mathrm{mm} 2\right)$. $\sigma_{s}$ is the design tension of PE100, in $N / \mathrm{mm}^{2} \sigma_{s}=$ MRS / C. MRS is the minimum tension required ( 10 MPa for PE100). C is the design coefficient $(1.25$ for water and 2 for gas). $\Delta L_{b 1}$ is the increase in length of the stretch $L_{b}$,

Example:
A 90 mm diameter and 5 m length pipe is to be installed to carry water under an estimated maximum temperature difference of $25^{\circ} \mathrm{C}$.

$$
\Delta \mathrm{L}_{1}=q * \Delta \mathrm{~T} * \mathrm{~L}=0.2 * 25 * 5=25 \mathrm{~mm} \quad \sigma_{\mathrm{s}}=\frac{\mathrm{MRS}}{\mathrm{C}}=\frac{10}{1.25}=8
$$

$$
\mathrm{L}_{\mathrm{b} 1}=\sqrt{\frac{3 * \mathrm{DN} * \Delta \mathrm{LL} * \mathrm{E}_{50}}{0.15 * \sigma_{\mathrm{s}}}}=\sqrt{\frac{3 * 90 * 25 * 150}{0.15 * 8}}=918.56 \mathrm{~mm}=0.92 \mathrm{~m}
$$

$\Delta \mathrm{L}_{\mathrm{b} 1}=\alpha * \Delta \mathrm{~T} * \mathrm{~L}=0.2 * 25 * 0.92=4.6 \mathrm{~mm}$

$$
\mathrm{L}_{\mathrm{b} 2}=\sqrt{\frac{3_{*} \mathrm{DN} * \Delta \mathrm{~L}_{\mathrm{b} 1} * \mathrm{E}_{50}}{0.15 * \sigma_{\mathrm{s}}}}=\sqrt{\frac{3 * 90 * 25 * 150}{0.15 * 8}}=176.21 \mathrm{~mm}=0.18 \mathrm{~m}
$$

## FLEXIBILITY. CURVATURE 13.3

The exposed installations must be installed on supports, to prevent serpentine effects, memory of the pipe due to being rolled up, etc.
Concerning lineal expansions, fixed points and moving points have already been discussed. In both cases, clamps that hold the pipe are installed. The former do not allow movement and the latter allow movement to absorb expansion.


Depending on where the installation is going to be placed, it may be advisable to place it on tiles or profiles. In all cases, the fastening or supporting elements of the pipes must be free of sharp edges that could damage the pipes.


As a guideline, a table with the recommended distance between supports is included. These values are for $20^{\circ} \mathrm{C}$, in case of reaching higher temperatures,

## the following reducer factors should be applied:

- From 20 to $35^{\circ} \mathrm{C}$, coefficient $=0.9$

From 35 to $40^{\circ} \mathrm{C}$, coefficient $=0.85$


The good flexibility of PE enables installations with a certain cold curvature without the need for fittings. The estimated calculations are based on the following equations:

$$
\begin{array}{lc}
\text { For low nominal pressures } & \text { For high nominal pressuresalta } \\
\mathrm{R}_{\mathrm{c}}=\mathrm{R}_{\mathrm{m}}{ }^{2} /(0.28 \star \mathrm{e}) & \mathrm{R}_{\mathrm{c}}=(0.5 \star \mathrm{OD})^{2} /
\end{array}
$$

where: $R_{c} \quad$ is the curvature ratio in $m m$
$\mathrm{R}_{\mathrm{m}} \quad$ is the medium ratio of the piping in mm
e is the thickness of the pipe in mm
OD is the outer diameter of the pipe in mm
$\varepsilon \quad$ is the elongation of the superior fibres, in percentage, and mustn't be higher than $2.5 \%$ in the long term

In general, you can use the following table with the values calculated at $20^{\circ} \mathrm{C}$. If the installation is done at $0^{\circ} \mathrm{C}$ it is multiplied by 2.5 ; and between 0 and $20^{\circ} \mathrm{C}$ a linear extrapolation is done:


### 13.4 PRESSURE DROP

,
To calculate the pressure drop in polyethylene piping, the Connor
or Colebrook abacus can be used, which relate the pressure drop to
speed, internal diameter and flow rate. In any case, UNE 53959 IN can
also be consulted.

Connor Graph

PRESSURE DROP J (m.c.a./ 100 m .)

The following coefficients are accepted depending on the equation
used for the calculation:
$\mathrm{k}=0.003 \mathrm{~mm}$ (absolute roughness, Colebrook formula)
$\mathrm{n}=0.008$ (Manning formula)
C $=150$ (Hazen Wiliams formula)


- Colebrok Graph


When a liquid is flowing through a piping at a constant speed and at a given time any element on the installation is operated (a valve is closed or opened, variation of a pump's speed, etc) an overpressure is caused, resulting in an unbalance in the fluidity speed of the liquid that alters flows and pressures in the different points of the pipeline. This overpressure is called water hammer and must be added to the working or service pressure.

Pressure and flow rate variations that result in a water hammer spread throughout the liquid mass in a wave-like motion. Wave propagation velocity is called celerity and is according to the water modulus of elasticity whose value varies according to the temperature and modulus of elasticity of the piping material.

The lower the value of the modulus of elasticity of the piping material, the lower the celerity and the overpressure value that can take place in the piping. It is therefore advisable to use polyethylene piping, due to their low modulus of elasticity, so as in the same operating conditions, they result in pressures that are much lower than those that would be produced with the use of classic materials, which are considerably more rigid.

Calculation of the overpressure by water hammer can be done using Michaud's equation:

$$
\begin{gathered}
\Delta \mathrm{H}= \pm \frac{2_{\star} \mathrm{L}_{\star} \mathrm{V}}{\mathrm{~g} * \mathrm{~T}} \\
\text { for } \\
\mathrm{T}>\frac{2{ }_{\star} \mathrm{L}}{\mathrm{a}}
\end{gathered}
$$

If: $\Delta \mathrm{F}=$ increase of pressure or height, or water hammer (overpressure in m.w.c.)
$a=$ wave propagation velocity or celerity in $\mathrm{m} / \mathrm{s}$
$\mathrm{r}=$ water velocity in a constant speed of $\mathrm{m} / \mathrm{s}$
$L=$ piping length in $m$
$\mathrm{g}=$ acceleration of gravity in $\mathrm{m} / \mathrm{s} 2 \mathrm{~T}=$ stop operation time in s
$\mathrm{T}=$ stopping manoeuvre time in s

The celerity is calculated with the equation:

$$
a=\frac{9900}{\sqrt{48.3+K_{c} * D_{m} / e}}
$$

$$
\mathrm{K}_{\mathrm{c}}=\frac{10^{10}}{\mathrm{E}}
$$

## If $\mathrm{Kc}=$ dimensionless indicato

$\mathrm{E}=$ piping modulus of elasticity in $\mathrm{kg} / \mathrm{M}^{2}\left(\mathrm{I}^{1} 0^{8}\right.$ for PE$)$
In the case of very long pipelines, the water hammer does not reach its maximum value at the closing end (or point of change of direction), but at a generic point inside the pipe. In this case the Allievi equation is used:

$$
\Delta \mathrm{H}= \pm \frac{\mathrm{a}{ }_{\star} \mathrm{v}}{\mathrm{~g}}
$$

if
$\mathrm{T}<\frac{2{ }_{\star} \mathrm{L}}{\mathrm{a}}$

The water hammer can be mitigated in different ways:

- Check valves. They are installed in the impulsions to protect in group of pumping and the emptying of the piping through the pump. They can also be placed on the pipeline operating pressure - Flywheel. Or pumping group stop delayer. By means of a flywheel attached to the motor shaft
Air tank. A tank attached to the piping in which there is water and air under pressure.
This air absorbs the pressure variations in the pipeline. Requires
maintenance as air dissolves in water over time
- Surge tank. A vertical tank attached to the piping and higher than the equivalent pressure the piping can withstand.
Air release valves. Prevents cavitation at high points in the installation
Safety valves. If there is a possibility of cavitation leading to strong overpressure
- Internal pressure test (hydrostatic pressure)

The hydrostatic pressure tests will be carried out in piping sections of less than 500 m in length, and will be carried out as the assembly is completed in each section, without waiting to have the entire work completed. The pressure difference between the highest and lowest point shall not exceed $10 \%$ of the test pressure.

The internal hydrostatic pressure for the trench test must never exceed 1.4 times the maximum working pressure of the piping at the lowest point of the section. The pressure shall be raised slowly, not exceeding $1 \mathrm{~kg} / \mathrm{cm} 2$ per minute.

Before starting the test, all the pipeline fittings must be placed in their final position and the piping will be conveniently anchored in all the changes of direction as well as in the fixed points. The anchoring must be designed to withstand the maximum thrust developed during hydrostatic testing. The trench must be partially filled, in order to avoid piping movements, always leaving the connections uncovered.

Start by slowly filling the section to be tested with water, leaving open all the elements for air outlet, which will then be closed successively from bottom to top, once it has been verified that there is no air in the pipeline. If possible, the water will enter from the lower part, which will make the air release from the upper part easier. If this is not possible, filling will be done even slower to avoid air remaining in the piping.
At the highest point of the pipeline, a bleeder valve will be placed to expel the air and to check that the whole section to be tested is properly communicated.

Once the entire section has been filled, an initial inspection will be
Tests according to UNE-EN 805
As an option, the test can be performed according to the UNE-EN 805 standard. This test is longer as it consists of three stages, following the attached chart:

- Preliminary or Relaxation Stage
- Pressure Drop Stage
- Main Stage
carried out to check that all the connections are leak-tight.
The equipment necessary for the pressure test must have the appropriate elements to regulate the pressure increase. It must be placed at the lowest point of the piping to be tested and must be fitted with pre-calibrated pressure gauges. The pressure will be raised but it mustn't exceed $1 \mathrm{bar} / \mathrm{min}$

The ends of the section to be tested will be conveniently closed and easily detachable in order to be able to continue assembling the piping once the test is finished

Once the pressure testing has been obtained, a 30 -minute pause will be made. The test will be considered satisfactory when during this time the pressure gauge does not indicate descent above $\downarrow$ ( p 5 ), being $p$ the pressure testing in trench in bar. When the pressure gauge drop is higher, leaks will be corrected and a new test will be carried out until a satisfactory result is obtained.

Various methods can be used to repair leaks or damaged sections. In general, the best way is to cut the damaged section and replace it with a prefabricated unit or fittings. When failure or damage occurs in a welded joint, the original weld must be completely eliminated before being re-welded.


## CONNECTION SYSTEMS

14.3 Electrofusion connect
14.4 Flanged systems
14.5 Mechanical systems
14.6 Systanch systems
14.7 System repai

The main connection system are:
Thermofusion or socket welding (recommended option)
Electrofusion.
Butt or mirror welding.
Others: Flanged fittings, threads, victaulic system, etc.
For most of these systems, there are a series of common points to keep in mind:
tisessentialto mind hecleaniness of he lewenstobe correded. Suct cleaning shoul never be done using chemicals. Wiping off any dirt with a clean cloth would be enough. The cuts of the parts to be joined must be as parallel as possible to each other and as perpendicular as possible to the length of the pipe. If there is any burr, it is advisable to remove it before connecting the parts.
In processes where temperature is involved, it is important to ensure that materials with similar melting points are to be connected.
It is necessary to take into account the environmental conditions where the connection is going to take place, since extreme temperatures could distort machine data in automatic welds, or even affect the elements to be connected. In the same way, it is necessary to avoid air currents that can make the connection difficult, since it may accelerate the partial cooling of the different elements.
14.1 THERMOFUSION OR SOCKET WELDING

The process consists of connecting a pipe and a fitting by applying heat on the external part of the pipe and the internal part of the fitting. To do this, the pipe is inserted into the heating matrix while anothe heating matrix is inserted into the fitting.

Once the corresponding time has elapsed (see time table), the matrices are removed and the pipe is inserted into the fitting, keeping the pressure for the indicated time.

This type of welding guarantees a perfect pipe - fitting connection. The end result is a single part, eliminating the risk of leakage.


Apply the matrices to the pipe and fitting

Steps for machine welding


## BUTT WELDING CONNECTION 14.2

| Warm-up time (s) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Nominal } \\ & \text { Diameter }(\mathrm{mm}) \end{aligned}$ | PN10 | PN16 | PN20 |  |  |
| 16 | --- | 3 | 5 | 4 | 10 |
| 20 |  | 3 | 5 | 4 | 10 |
| 25 | --- | 4 | 6 | 4 | 15 |
| 32 | --- | 5 | 7 | 6 | 15 |
| 40 | --- | 7 | 10 | 6 | 25 |
| 50 | 9 | 11 | 15 | 6 | 25 |
| 63 | 12 | 14 | 20 | 8 | 40 |
| 75 | 18 | 20 | 25 | 8 | 40 |
| 90 | 25 | 30 | 35 | 8 | 50 |
| 110 | 35 | 45 | 45 | 10 | 60 |
| 125 | 40 | 50 | 50 | 10 | 65 |

Note: 11 is recommended to wait at least a couple of hours before testing for leaks.

## - Special care of the heating matrices

It is important to keep them in good condition, preventing them from suffering any impact or scratches.
Always keep them clean. If there is any material attached left, remove it while they are still hot using a clean cloth.
If they are used for more than one material, cleaning when finished is especially important.

If they are damaged, replace them with new ones. The matrices have a Teflon coating which ensures a homogeneous distribution of heat. If the Teflon is damaged, the matrix will not heat evenly in all its parts and correct welding cannot be guaranteed.

The procedure consists of heating two pipes (or a pipe with an fitting of the same outer diameter and thickness as the pipe) by means of a heating plate (approximately $210-225^{\circ} \mathrm{C}$ ), and then use pressure to achieve the connection of the two elements.
It is usually used for large diameters. It is very important to carry this out using equal thicknesses and diameters.
Welding instructions

- Place the elements aligned on the welding machine.
- Face the pipes (using the blade of the machine itself) to properly clean the surfaces and even them out.
- Remove the facing tool and the burrs without touching the surfaces to be connected.
Ensure the surfaces are parallel to each other.
- Check that the heating plate is clean and at the correct temperature.
- Follow the pressure curve indicated by the machine manufacturer
- A first Pl pressure is exerted for a Tl time to create the initial height cord (h).
- After this time, lower the pressure to ensure full heating P2 (preset

After the heating time T2, move back the elements and remove the heating plate and quickly connect the ends T3.
Increase the pressure progressively until it reaches the pressure indicated by the manufacturer P1 - T4.
Maintain this pressure for the time indicated until the weld is cold
T5.
Wait about two hours before doing hydraulic tests.


ALIGNMENT
Maximum allowable deviations


Initial cord height in a ${ }^{*} T$, tim




The system consists of passing a low voltage current throug metal coils inside the fittings, embedded in the polypropylene, causing the Joule heating effect that welds the fitting with the pipe previously inserted in it.

inserted without forcing it but play-free)


Read fitting label code


Reboca, S.L. has flanged systems that enable the connection between pipes. REPOLEN flanges are PN16.
Remember that the screws tightening must always be done crosswise and gradually, to ensure a perfect coupling of the gasket.


It consists in using mechanical fittings, normally threaded. It is usually used for small diameters and thicknesses.

The assembly steps are:

- Cut the pipe perpendicularly
- Disassemble the fitting to be connected
- Insert the pipe by butt pressure
- Retighten the fitting thread

MECHANICAL SYSTEMS 14.5



Make a hole in the pipe where you want to make the new intake with the corresponding drill


Apply the heating matrices both to the pipe and to the branch to be grafted, proceeding in the same way as with any socket weld



Cut the edges that may remain carefully so as not to damage the pipe


Remove the matrices and insert the branch into the hole
to solve it.



Insert the plug into the hole taking care not to insert it too much so as not to create turbulence in the water flow



ANNEXES

### 9.1 CHEMICAL RESISTANCE TABLE

| + Resists with insignificant variations <br> / Resists with variations under certain conditions <br> - Does not resist |  |  |  | cold sat. Cold saturation <br> e Boiling <br> a Aqueous solution |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Product | coscraturos | тмmmutrus |  | Product |  | concasmantos | temparvis |  |
|  |  | $20^{\circ} \mathrm{C}$ | $60 . \mathrm{C}$ |  |  |  | 200 C | $60 \cdot \mathrm{C}$ |
| Coconut oil |  | + | 1 | Citric acid |  | saturated | + | + |
| Flaxseed oil | 100 | + | + | Hydrochloric acid |  | 10-35 | + | + |
| Corn oil | 100 | + | 1 |  |  | concentrated | + | + |
| Paraffin oil | 100 | + | + | Chlorous acid |  | concentrated | + | + |
| Castor oil | 100 | + | + | Chlorosulfuric acid |  | 100 | - | - |
| Silicone oil | 100 | + | + | Cresylic acid |  | 50 | + | + |
| Diesel | 100 |  |  | Chromic acid |  | 50 | + | 1 |
| Heating oil | 100 | + | 1 |  |  | 80 | + | - |
| Fine spindle oil | 100 | 1 | 1 | Dichloroacetic acid |  | 50 | + | + |
| Engine oils | 100 | + | 1 |  |  | 100 | + | 1 |
| Animal oil |  | + | 1 | Stearic acid |  | 100 | + | 1 |
| Ethereal oils |  | 1 | 1 | Ethylenediaminetetraac | ic acid |  | + | + |
| Mineral oils | 100 | + | 1 | Fluoric acid |  |  | + | + |
| Vegetable oil |  | + | 1 | Hydrofluoric acid |  | 40-40 | + | 1 |
| Acetaldehyde | 100 | + | 1 | Fluorosilicic acid |  | 32 | + | + |
| Ammonium acetate |  | + | + |  |  | Conc. Sol. | + | + |
| Amyl acetate | 100 | + | 1 | Formic acid |  | 10-80 | + | + |
| Butyl acetate | 100 | + | 1 |  |  | 100 | + | 1 |
| Ethyl acetate | 100 | 1 | 1 | Phosphoric acid |  | 0-30 | + | + |
| Methoxybutyl acetate | 100 | + | 1 |  |  | 30-90 | + | + |
| Lead acetate | Saturated | + | + |  |  | 95 | + | 1 |
| Acetone | 100 | + | + | Phthalic acid |  | 50 | + | + |
| Acetic Acid | 1-10 | + | + | Gallic acid |  | saturated | + | 1 |
|  | 10-60 | + | 1 | Glycolic acid |  | 30 | + | + |
|  | 80-100 | + | 1 |  |  | 55 | + | + |
| Adipic acid |  | + | + |  |  | 70 | + | + |
| Aminoacetic Acid |  | + | + | Hypochlorous acid |  | conc | + | 1 |
| Aromatic Acids |  | + | + | Lactic acid |  | 10-80 | + | + |
| Arsenic Acid | 100 | + | + |  |  | 90-100 | + | 1 |
| Benzenesulfonic acid |  | + | + | Maleic acid |  |  | + | + |
| Benzoic acid | Aqueous Sol. | + | + | Malic acid |  | 50 | + | + |
| Boric acid | Sol. | + | + | Methylsulfuric acid |  |  | + | 1 |
| Bromhydric acid | 10-50 | + | + | Monochloracetic acid |  |  | + | + |
| Butyric acid |  | + | 1 | Nicotinic acid |  |  | + | + |
| Carbonic acid (dry / wet) | 100 | + | + |  |  |  |  |  |
| Hydrocyanic acid | saturated | + | + |  |  |  |  |  |


| Product | coscestaros |  |  | product | coscasmurox | tmamunut |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $20^{\circ} \mathrm{C}$ | $6{ }^{60}$ |  |  | $20^{20}$ |  |
| Nitric acid | 0-30 | + | + | Camphor |  | + | 1 |
|  | 30-50 | + | 1 |  | crystals | + | 1 |
|  | 70 | + | 1 |  | oil | - | - |
|  | 98-98 |  |  | Ally alcohol | 96 | + | + |
| Oleic acid | conc | + | 1 | Amyl alcohol | 100 | + | - |
| Oxalic acid | diluted | + | + | Benzyl alcohol |  | + | + |
|  | saturated | + | + | Butyl alcohol |  | + | + |
| Perchloric acid | 20 | + | + | Ethyl alcohol | 100 | + | + |
|  | 50 | + | 1 | Furfuryl alcohol | 100 | + | 1 |
|  | 70 | + |  | Isobuty lalcohol |  | + | + |
| Picric acid |  | + | + | Isopropyl alcohol |  | + | + |
| Propionic acid | 50 | + | + | Methyl alcohol |  | + | + |
|  | 100 | + | 1 | Glycolic Alcohol |  | + | 1 |
| Salicylic acid |  | + | + | Propyl alcohol |  | + | + |
| Selenic acid |  | + | + | Starch | saturated | + | + |
| Silicic acid |  | + | + | Chromium Alums | saturated | + | + |
| Sodium Acid | saturated | + | + | Ammonia | dry gas 100 | + | + |
| Succinic acid | 50 | + | + |  | liquid | + |  |
| Hydrogen sulphide |  | + | + |  | solution | + | + |
| Sulphochromic acid |  |  | - | Acetic anhydride |  | + | 1 |
| Sulphuric acid | 0-50 | + | + | Carbon dioxide | dry 100 | + | + |
|  | 70 | + | 1 |  | wet | + | + |
|  | 80 | + | - | Phosphoric anhydride |  | + | + |
|  | 96 | 1 | - | Phthalic anhydride |  | + | + |
|  | 98 | 1 | - | Sulphuric anhydride |  | 1 | - |
|  | oleum | - | - | Sulphur dioxide | wet | + | + |
| Sulphuric acid | 10 | + | + | Aniline | 100 | + | 1 |
| Tannic acid | 10 | + | + | Arsenic |  | + | + |
| Tartaric acid | 10 | + | + | Aspirin |  | + | + |
|  | saturated | + | 1 | Sulphur | colloidal | + | + |
| Trichloroacetic acid | 50 | + | + | Galvanic baths |  | + | + |
|  | 100 | + |  | Benzene | 100 | 1 | - |
| Fatty acids with more than 4 carbon atoms |  | + | 1 | Benzine | 100 | 1 | - |
| Acrylonitrile | 100 | + | + | Benzaldehyde |  | + | 1 |
| Chlorine water | 2 | + | + | Sodium benzoate | saturated | + | + |
| Sea water |  | + | + | Potassium bicarbonate | saturated | + | + |
| Hydrogen peroxide | 30 | + | , | Sodium bicarbonate | saturated | + | + |
|  | 90 | + | - | Potassium dichromate | saturated | + | + |
| Aqua regia |  | - | - | Sodium dichromate | saturated | + | + |
|  |  |  |  | Sodium bisulphate | saturated | + | + |
|  |  |  |  | Sodium bisulfite | saturated | + | + |

Bromine
Aromochloromethane
Calcium bromide
Potassium bromide
Butadiene
Butanediol
Butylene Glycol
Coffee
Cinnamon

|  | oil |  |  |
| :---: | :---: | :---: | :---: |
| Ammonium carbonate |  | + | + |
| Calcium carbonate |  | + | + |
| Barium carbonate | saturated | + | + |
| Bismuth carbonate | saturated | + | + |
| Magnesium carbonate | saturated | + | + |
| Potassium carbonate |  | + | + |
| Sodium carbonate | solution | + | + |
| Beeswax |  | + | 1 |
| Beer |  | + | + |
| Ketones | 100 | + | 1 |
| Copper cyanide |  | + | + |
| Mercury cyanide | saturated | + | + |
| Potassium cyanide | saturated | + | + |
| Sodium cyanide | saturated | + | + |
| Cyclohexane |  | + | + |
| Cyclohexanol |  | + | 1 |
| Cyclohexanone |  | + | 1 |
| Calcium chlorate | saturated | + | + |
| Barium chlorate | saturated | + | + |
| Potassium chlorate | saturated | + | + |
| Sodium chlorate | saturated | + | + |
| Sodium chlorite | 50 | + | + |
| Chlorine | wet gas | 1 | - |
|  | dry gas | 1 | - |
|  | liquid 100 | - | - |
| Chlorobenzene |  | 1 | - |
| Chloroethanol |  | + | + |
| Chloroform | 100 | 1 | - |

Chloroform
100

| Aluminium chloride | solution | + | + |
| :---: | :---: | :---: | :---: |
| Amyl chloride | 100 | / | - |
| Ammonium chloride | solution | + | + |
| Antimony chloride | saturated | + | + |
| Barium chloride | saturated | + | + |
| Benzoyl chloride |  | 1 | / |
| Calcium chloride | solution | + | + |
| Zinc chloride | solution | + | + |
| Copper chloride | solution | + | + |
| Tin chloride | saturated | + | + |
| Ferrous chloride | saturated | + | + |
|  | solution | + | + |
| Ferric chloride | solution | + | + |
| Magnesium chloride | solution | + | + |
| Mercuric chloride | sublimated | + | + |
|  | solution | + | + |
| Methylene chloride | 100 | , | / |
| Nickel chloride | saturated | + | + |
| Potassium chloride | solution | + | + |
| Sodium chloride | solution | + | + |
| Sulphuryl chloride |  | - | - |
| Thionyl chloride |  | - | - |
| Creosote |  | + | + |
| Cresol |  | + | + |
| Potassium chromate | saturated | + | + |
| Shampoo |  | + | + |
| Decalin | 100 | / | - |
| Disinfectants |  | + | - |
| Synthetic detergents | solution | + | + |
| Dextrin | saturated | + | + |
| Dextrose | saturated | + | + |
| Methyl dichloroacetate |  | + | + |
| Dichloroethane |  | ' | , |
| Dichloroethylene |  | - | - |
| Potassium dichromate | saturated | + | + |
| Sodium dichromate | saturated | + | + |
| Diethylene glycol |  | + | 1 |
| Diisobutylketone |  | + | - |
| Diethanolamine |  | + | 1 |
| Dimethylformamide |  | + | 1 |
| Dioxane | 100 | + | + |
| Carbon dioxide | saturated cold | + | + |
|  | wet 100 | + | + |
|  | dry 100 | + | + |

## Emulsifiers

Acrylic Emulsions
Photographic emulsions
Epichlorohydrin
Turpentine Essence
Whale sperm
Aliphatic esters

## Ethanol <br> Ethanol

$$
100
$$

## Ether

Petroleum Ether
Dibutyl ether
Diethyl ether
Ethyl ether
Isopropyl ether
Ethylbenzene
Ethylene glycol
Tanning extracts
Orange extracts
Vanilla extracts
Phanacetin
Phenylsulfonate
Phenol

|  |  | + | + |
| :--- | :--- | :--- | :--- |
| Potassium ferricyanide | saturated | + | + |
| Sodium ferricyanide | saturated | + | + |
| Fluorine |  | - | - |

Ammonium fluoride

|  | 70 | + | + |
| :--- | :---: | :---: | :---: |
| Aluminium fluoride |  | + | + |
| Copper Fluoride | saturated | + | + |
| Potassium fluoride | saturated | + | + |
| Sodium fluoride | saturated | + | + |
| Formaldehyde | $10-30$ | + | + |
|  | $30-40$ | + | + |
| Phosphine | 100 | + | + |
| Ammonium phosphate |  | + | + |
| Tri-b-chloroethylene phosphate |  | + | + |
| Tributyl phosphate |  | + | + |
| Tricesyl phosphate | 100 | + | + |
| Disodium phosphate |  | + | + |
| Sodium phosphate |  | + |  |
| Trisodium phosphate |  |  | + |
|  | saturated | + | + |


| Product | concesmunow | тменаития |
| :---: | :---: | :---: |
|  |  | 60 C |
| Yellow phosphorus | 100 | + + |
| Fructose | saturated | + + |
| Dibutyl phthalate | 100 | + 1 |
| Furfural | 100 | 1 - |
| Natural gas |  | + + |
| Nitrous gases |  | + + |
| Diesel |  | + - |
| Petroleum jelly |  | + + |
| Glycerine. | solution | + + |
| Glycol | concentrated | + + |
| Butyl glycolate |  | + + |
| Glucose |  | + + |
| Heptane |  | 1 - |
| Hexachlorobenzene |  | + + |
| Hexane | 100 | + 1 |
| Hexanol | 100 | 1 - |
| Chloral hydrate | solution | + + |
| Hydrazine hydrate |  | + + |
| Aromatic hydrocarbons |  | 1 - |
| Hydrogen | 100 | + + |
| Hydroquinone |  | + + |
| Hydrosulphite | 10 | + + |
| Ammonium hydroxide | p.c. 0.88 | + + |
| Calcium hydroxide | saturated | + + |
| Barium hydroxide | saturated | + + |
| Magnesium hydroxide | saturated | + + |
| Potassium hydroxide | concentrated | + + |
|  | 20 | + + |
|  | 50 | + + |
| Sodium hydroxide | 30 | + + |
|  | concentrated | + + |
| Calcium hypochlorite | 15\% Active Cl | + + |
| Sodium hypochlorite |  | + + |
| Iodine |  | + + |
| Isooctane |  | + 1 |
| Isopropanol |  | + + |
| Syrups | usual | + + |
| Kerosene |  | 1 / |
| Lanolin |  | + + |
| Latex |  | + + |
| Milk |  | + + |
| Bleach | 15\% act. | + + |
| Yeast |  | + + |
| Hydraulic Liquid |  | + 1 |

Methanol
4-methyl-2-pentanol Methylcyclohexane Methyl ethyl ketone
Methylglycol
Methoxybutanol
Sulphochromic mixture
Methyl monochloroacetate
Carbon monoxide
Morpholi
Naphtha
Naphthalene
Ammonium nitrate
Calcium nitrate
Magnesium nitrate
Mercury nitrate
Nickel nitrate
silver nitrate
Ferric nitrate
Potassium nitrate
Sodium nitrate
o-dichlorobenzene
Oleum
${ }^{\mathrm{o}}$-nitrotoluene
Phosphorus oxychloride
Carbon Oxide
Zinc oxid
Oxygen
-dochlorobenze
Phosphorus pentoxide
Potassium perborate
Sodium perborate Potassium perchlorate
Perchlorethylene

$\qquad$
saturated
saturated saturarated
saturated
saturated
saturated solution

|  | - | - |
| :---: | :---: | :---: |
|  | + | 1 |
|  | + | 1 |
|  | + | + |
|  | + | + |
| 100 | + | 1 |
| 100 | 1 | - |
|  | 1 | - |
| 100 | + | + |
| saturated | + | + |
|  | + | + |
| saturated | + | + |
| 100 | 1 | - |


| product | сомсалтмток | тмшгм |
| :---: | :---: | :---: |
|  |  | 20.0 |
| Potassium permanganate | 6 | + + |
|  | 20 | + + |
| Sodium peroxide | 10 | + |
|  | saturated | 1 |
| Ammonium persulphate | saturated | + + |
| Potassium persulphate |  | + + |
| Petroleum |  | + 1 |
| Pyridine |  | + 1 |
| Tetraethyl lead | 100 | 1 1 |
| Polyglycols |  | + + |
| Caustic Potash |  | + |
| Propane | gas | + + |
| Propylene glycol |  | + 1 |
| Pseudocoumene |  | 11 |
| Fruit pulp |  | + |
| p -Xylene | 100 | 1 - |
| Resorcinol |  | + |
| Photographic developers |  | + + |
| Common salt | saturated | + |
| Brine | saturated | + |
| Tallow |  | + |
| Cider |  | + |
| Sodium silicate | solution | + |
| Caustic soda |  | + |
| Aluminium sulphate | solution | + |
| Ammonium sulphate | saturated | + |
| Barium sulphate | saturated | + |
| Calcium sulphate |  | + |
| Zinc sulphate | saturated | + + |
| Copper sulphate | saturated | + |
| Ferrous sulphate |  | + + |
| Magnesium sulphate | saturated | + |
| Nickel sulphate | saturated | + |
| Potassium sulphate | concentrated | + + |
| Sodium sulphate | concentrated | + |
| Barium Sulfite | saturated | + |
| Potassium sulphite | concentrated | + |
| Sodium sulphite | saturated | + + |
| Dimethyl sulfoxide |  | + + |
| Ammonium sulphide | saturated | + + |
| Barium sulphide | saturated | + + |
| Calcium sulphide |  | + + |
| Carbon sulphide | 100 | 1 - |


|  |  | $20^{\circ} \mathrm{C}$ |  |
| :---: | :---: | :---: | :---: |
| Potassium sulphide | concentrated | + | + |
| Sodium sulphide | 25 | + | + |
|  | saturated | + | + |
| Talcum | 100 | + | + |
| тea |  | + | + |
| Tetrabromoethane |  | - | - |
| Tetrachloroethane |  | 1 | - |
| Tetrachloroethylene | 100 | 1 | - |
| Carbon tetrachloride | 100 | + | / |
| Tetrahydrofuran | 100 | + | 1 |
| Tetraline | 100 | + | / |
| Tincture of iodine |  | + | 1 |
| Ammonium thiocyanate | saturated | + | + |
| Thiophene |  | , | / |
| Sodium thiosulphate | saturated | + | + |
| Toluene | 100 | 1 | - |
| Trichloroethylene | 100 | - | - |
| Antimony trichloride |  | + | + |
| Phosphorus trichloride | 100 | + | 1 |
| Trielanolamine | 100 | + | - |
| Urea | 33 | + | + |
| Vaseline |  | 1 | 1 |
| Vinegar | commercial | + | + |
| Wine |  | + | + |
| White spirit |  | 1 | 1 |
| Apple juice |  | + | + |
| Orange juice |  | + | + |
| Tomato juice |  | + | + |
| Grape juice |  | + | + |
| Carrot juice |  | + | + |

Hikepolen


## ) Repolen

PRODUCT MANUFACTURED AND DISTRIBUTED BY
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